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Optimal Pore Chemistry in an Ultramicroporous Metal–Organic Framework for Benchmark Inverse CO₂/C₂H₂ Separation

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Abstract: Isolation of CO_2 from acetylene (C_2H_2) via CO_2 selective sorbents is an energy-efficient technology for C_2H_2 purification, but a strategic challenge due to their similar physicochemical properties. There is still no specific methodology for constructing sorbents that preferentially trap CO_2 over C_2H_2 . We report an effective strategy to construct optimal pore chemistry in a Ce^{IV}-based ultramicroporous metalorganic framework Ce^{IV}-MIL-140-4F, based on charge-transfer effects, for efficient inverse CO_2/C_2H_2 separation. The ligandto-metal cluster charge transfer is facilitated by Ce^{IV} with lowlying unoccupied 4f orbitals and electron-withdrawing F atoms functionalized tetrafluoroterephthalate, affording a perfect pore environment to match CO_2 . The exceptional CO_2 uptake $(151.7 \text{ cm}^3 \text{ cm}^{-3})$ along with remarkable separation selectivities (above 40) set a new benchmark for inverse CO_2/C_2H_2 separation, which is verified via simulated and experimental breakthrough experiments. The unique CO₂ recognition mechanism is further unveiled by in situ powder X-ray diffraction experiments, Fourier-transform infrared spectroscopy measurements, and molecular calculations.

Introduction

Acetylene (C_2H_2) is one of the predominant precursor chemicals. It is mainly produced by partial combustion of natural gas and steam cracking of hydrocarbons, with a significant contaminant of CO₂ unavoidably co-generated.^[1] Therefore, the separation of CO₂ from C₂H₂ is essential in the petrochemical industry to obtain high-purity C₂H₂. However, both C₂H₂ and CO₂ are non-polar. They have very similar physicochemical properties (boiling points of 189.3 and 194.7 K for C₂H₂ and CO₂, respectively) and almost identical size and dimension (kinetic diameter of 3.3 Å for both gases; $3.3 \times 3.3 \times 5.7$ Å³ for C₂H₂ and $3.2 \times 3.3 \times 5.4$ Å³ for CO₂; Supporting Information, Figure S1), undoubtedly giving rise to a daunting challenge for their separation.^[1a-d] The

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 CO_2/C_2H_2 separation process is implemented primarily by energy-intensive approaches, such as solvent extraction and cryogenic distillation. Adsorptive separation using porous adsorbents is a promising alternative technology, which is more environmentally friendly and energy-efficient than the heat-driven processes. However, the close similarities and the strict upper compression limit of C_2H_2 (2 bar) handicap the utilization of conventional porous materials, such as zeolites and carbon materials, for CO_2/C_2H_2 separation.^[2] Thus, the development of novel porous materials for the efficient isolation of CO_2 from C_2H_2 is highly urgent yet challenging.

Metal-organic frameworks (MOFs) or porous coordination polymers (PCPs), self-assembled by inorganic metal nodes or clusters with organic ligands, have emerged as a new class of crystalline porous materials,^[3] and offered a unique platform for addressing the challenges of gas separation.^[4] Judicious design of the pore size/shape and pore chemistry by the modular nature of MOFs based on crystal engineering and reticular chemistry endows some MOFs with unprecedented adsorption and separation behaviors for light hydrocarbons, including C₂H₂/C₂H₄, C₃H₆/C₃H₈, C4 olefins, etc.^[4,5] The almost identical molecular size of CO2 and C2H2 renders it impractical and quite challenging for MOFs to discriminate them via fine-tuned pore size or shape. Numerous MOFs have been reported with substantial C₂H₂/CO₂ selectivity.^[1c] This is due to the ease of designing active sites in MOFs for extra interactions with guests, such as acid-base interaction and hydrogen-bonding interaction. In the context of C₂H₂ and CO₂ separation, the acidic H atoms with positive charge in C₂H₂ are capable of interacting strongly with these active sites, resulting in high C₂H₂/CO₂ selectivity.^[6] However, since CO_2 is the main contaminant in C_2H_2 (3% and even up to 50%),^[2e] CO₂-selective sorbents are preferred for C₂H₂ purification because they will permit the direct isolation of C_2H_2 as a pure raffinate product. This will also efficiently leverage extensive industrial expertise in light-product-focused adsorptive cycles.^[1c,2c] Unfortunately, MOFs exhibiting inverse CO_2/C_2H_2 selectivity are rare, and within this subset of materials, the trade-off between CO₂ adsorption capacity and inverse CO₂/C₂H₂ selectivity is still a significant barrier in prevailing materials. For example, SIFSIX-3-Ni,^[1d] CD-MOFs,^[7] and ionic crystals^[8] with CO₂ uptake capacities of 98.4, 60.4, and 27 cm³ cm⁻³ only exhibit CO_2/C_2H_2 (1/2) selectivity of 7.7, 6.6, and 4.8, respectively. Thus, novel MOFs with high CO₂ capacity and inverse CO₂/C₂H₂ separation selectivity are of paramount importance in C₂H₂ purification. However, seeking strategies to construct MOFs with preferential sorption of CO₂ over C₂H₂ is still in its infancy.

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Notably, there is a huge difference in quadrupole moment between CO_2 $(-13.4 \times 10^{-40} \text{ Cm}^2)^{[9]}$ and C_2H_2 $(+20.5 \times$ 10⁻⁴⁰ Cm², Figure S1),^[2d,10] enlightening us to judiciously tune the pore chemistry with inverse electrostatic potential to leverage the quadrupole moment difference between CO₂ and C_2H_2 , thus leading to inverse CO_2/C_2H_2 separation. For this reason, the metal node in MOFs should be in a high oxidation state to withdraw the electrons from ligands, producing a more polar pore surface to recognize CO₂ molecules preferentially. Accordingly, the strategy combining Ce^{IV} with unoccupied 4f orbitals and perfluorinated aromatic spacer, tetrafluoroterephthalate (TFBDC), meets such a request. Herein, we explored the framework, Ce^{IV}-MIL-140-4F, for inverse CO₂/C₂H₂ adsorption and separation, and compared its performance with the isostructural Zr^{IV}-MIL-140-4F, which is for the first time obtained and investigated. Notably, this pair of MOFs provides an interesting example of diverging sorption behaviors in isostructural frameworks, in which Ce^{IV}-MIL-140-4F exhibits excellent CO₂-preferential adsorption performance over C₂H₂, while Zr^{IV}-MIL-140-4F exhibits normal C₂H₂ selectivity over CO₂. Ce^{IV}-MIL-140-4F provides an optimal pore environment to match CO₂, and CO₂ is trapped into the pores via strong host-guest interactions by four F atoms from two linkers, which is evidenced by in situ powder X-ray diffraction (PXRD) and Fouriertransform infrared spectroscopy (FTIR) studies, as well as molecular simulations. As a result, Ce^{IV}-MIL-140-4F exhibits a superior CO₂ uptake of $151.7 \text{ cm}^3 \text{ cm}^{-3}$ at 273 K and excellent separation selectivities (above 40) for CO_2/C_2H_2 mixtures. In addition, breakthrough experiments and simulations further confirm the excellent CO_2/C_2H_2 separation performance. These results render Ce^{IV}-MIL-140-4F a new benchmark material for inverse CO2/C2H2 separation, which is highly sought in the industrial separation process but rarely seen in the current literature.

Results and Discussion

The microcrystalline powder of Ce^{IV}-MIL-140-4F was obtained via refluxing cerium(IV) ammonium nitrate and H₂TFBDC in water at 383 K for 24 h.^[11] Ce^{IV}-MIL-140-4F crystallizes in the monoclinic C2/c space group and possesses perfluorinated one-dimensional triangular pore channels, making it highly hydrophobic (Figure S2). The Ce^{IV} ions in Ce^{IV}-MIL-140-4F exhibit a seven-coordination mode with three bridging μ_3 -O oxygen atoms and four oxygen atoms from the dicarboxylic ligands, forming octahedral CeO7 dimers. This is distinct from the 12-connected hexanuclear $Ce_6O_4(OH)_4(COO)_{12}$ clusters with structural hydroxy groups in the UiO-66 analogs.^[11,12] The octahedra CeO₇ dimers are connected via the corner-sharing octahedra, leading to onedimensional (1D) inorganic chains or sub-building units running along the c axis (Figure 1a). The 1D chains are connected through six TFBDC moieties in perpendicular directions, constructing 1D triangular channels with abundant F atoms stretching into the pores with pore apertures of 3.4-4.3 Å (Figure 1b). This pore structure is different from that in MIL-47 with 1D lozenge-shaped channels. This is due to the different coordination number of Ce^{IV} (7) compared to V^{V} (6), and the presence of a complex "double chain" inorganic building units in Ce^{IV}-MIL-140-4F (Figure 1a) instead of a simple chain of corner-sharing octahedra in MIL-47.^[13] Bulk purity of Ce^{IV}-MIL-140-4F was established by comparing experimental PXRD patterns with those calculated from crystal data (Figure 1e). Replacing Ce^{IV} with Zr^{IV}, the perfluorinated analog Zr^{IV}-MIL-140-4F was obtained for the



Figure 1. a) One-dimensional inorganic subunit of the metal oxide chain in MIL-140-14F. b) Illustration of the crystal structure and pore chemistry of MIL-140-4F. c,d) The Hirshfeld surface with d_e (electrostatic potential) and binding sites in Ce^{IV}- (c) and Zr^{IV}-MIL-140-4F (d) (red-to-blue color indicates the high-to-low transition of electron density). e) Experimental and simulated PXRD patterns of Ce^{IV}-MIL-140-4F. f) Experimental (black) and Pawley refined (red) PXRD patterns of Zr^{IV}-MIL-140-4F.

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first time. The unit cell parameters (a = 25.8173, b = 11.6115, $c = 8.0821, \ \alpha = \gamma = 90, \ \beta = 96.0813$) were confirmed via the Pawley refinement of the PXRD patterns in conjunction with structural of acceptable fitting metrics: $R_{wp} = 5.4$ % and $R_p =$ 3.3% (Figure 1 f; Supporting Information, Table S1). The unit cell of Ce^{IV}-MIL-140-4F is relatively smaller than that of Zr^{IV}-MIL-140-4F, as a consequence of the high oxidation state of Ce^{IV} with empty 4f orbitals facilitating the formation of a compact network.^[11] To investigate the chemical properties of the channels and provide clues to the structure-property relationships, we analyzed the electrostatic potential distributions based on the Hirshfeld surface with d_e on MIL-140-4F materials (Figure 1 c,d).^[14] The two MIL-140-4F MOFs exhibited a particular electronic distribution on their pore surface, with two distinct electronic regions in the edges of the triangular channels, denoted as electron-rich site I (blue dotted line) and electron-poor site II (pink dotted line). It is worth noting that Ce^{IV}-MIL-140-4F exhibits a much higher electron cloud density on site I and more positive potentials on site II, compared to Zr^{IV}-MIL-140-4F. This may originate from the strong electron-withdrawing effect of Ce^{IV} with empty and low-lying 4f orbitals facilitating ligand-to-cluster charge transfer, and this process can be accelerated by the functionalization of ligands with electron-withdrawing groups.^[12a,c,d,15] Compared with the molecular properties of C_2H_2 and CO₂, it is expected that these two specific and distinct sites with inverse electron potential in MIL-140-4F can well match the inverse quadrupole moments of C₂H₂ and CO₂. Additionally, there is an obvious difference in pore electrostatic potential on site II between Ce^{IV}- and Zr^{IV}-MIL-140-4F, which means different host-guest interaction modes may be observed on site II for CO_2 and C_2H_2 adsorption.

Guest-free MIL-140-4F materials can be readily obtained at 100 °C in vacuo for 12 h, and thermogravimetric analyses demonstrated that Ce^{IV}-MIL-140-4F is thermally stable up to ca. 330 °C (Figure S3). Ce^{IV}-MIL-140-4F is chemically robust, being unaffected by soaking in water or exposing to air for prolonged periods, and even in strong acid solutions $(1.6 \text{ mol } \text{L}^{-1} \text{ of HNO}_3)$, as confirmed by the PXRD patterns and CO₂ sorption isotherms (Figures S4 and S5). The permanent porosity of MIL-140-4F materials was confirmed by N_2 sorption experiments at 77 K. They exhibit fully reversible type-I isotherms without hysteresis, which is characteristic of microporous materials with permanent microporosity (Figure S6). The Brunauer-Emmett-Teller (BET) surface area and pore volume of Ce^{IV}-MIL-140-4F were calculated to be $360 \text{ m}^2\text{g}^{-1}$ and $0.11 \text{ cm}^3\text{g}^{-1}$, respectively, relatively larger than that of Zr^{IV} -MIL-140-4F (314 m²g⁻¹ and $0.11 \text{ cm}^3 \text{g}^{-1}$, respectively). All the values of pore size (Figure S7), volume, and surface area of MIL-140-4F materials are smaller than those of the UiO series (Figure S6) due to the simple 1D pore systems of MIL-140.

Considering the unique pore chemistry associated with suitable pore aperture size, low-pressure CO_2 and C_2H_2 sorption isotherms of Ce^{IV_2} and Zr^{IV} -MIL-140-4F were collected and a marked difference in the sorption behavior for CO_2 and C_2H_2 was observed (Figure 2 a). Intriguingly, Ce^{IV} -MIL-140-4F exhibits an inverse CO_2 -selective sorption behavior over C_2H_2 . On the contrary, Zr^{IV} -MIL-140-4F

preferentially adsorbs C₂H₂ over CO₂. Due to the industrial emphasis on the volume rather than the weight of the adsorbent in stationary applications, the volumetric capacity is often a better indicator of gas uptakes.^[16] The CO₂ uptake of Ce^{IV} -MIL-140-4F is 110.3 cm³ cm⁻³ at 298 K, much higher than that of C_2H_2 (41.5 cm³ cm⁻³), giving rise to a CO_2/C_2H_2 uptake ratio of 2.66. At 273 K, CO₂ and C₂H₂ uptakes can reach 151.7 and 53.5 cm³ cm⁻³, respectively (Figure 2b). The uptake of CO₂ at 298 K is much higher than that of the most state-of-the-art CO₂-selective materials, such as MUF-16 $(74.7 \text{ cm}^3 \text{ cm}^{-3})$,^[2c] SIFSIX-3-Ni (98.4 cm³ cm⁻³),^[1d] PCP-NH₂-ipa (93.6 cm³ cm⁻³),^[17] and CD-MOFs (60.4 cm³ cm⁻³).^[7] At 273 K, the uptake is comparable with that of the benchmark Tm-OH-bdc (153 cm³ cm⁻³)^[18] (Figure 2c), suggesting the feasibility of Ce^{IV}-MIL-140-4F in inverse CO₂/C₂H₂ separation. Notably, detailed analysis shows that the CO₂ isotherm of Ce^{IV}-MIL-140-4F exhibits a stepwise-shaped profile, indicating its flexibility, which may come from the rotation of benzene rings upon CO₂ sorption.^[1a] The steep CO₂ isotherm at 273 K and the attainment of the plateau at low pressures indicate the strong affinity of the framework toward CO₂. Additionally, the 196 K isotherms of CO₂ and C₂H₂ further confirm the preferential adsorption performance of Ce^{IV}-MIL-140-4F for CO₂ over C₂H₂ (Figure 2d). In contrast, $Zr^{\mbox{\scriptsize IV}}\mbox{-MIL-140-4F}$ preferentially adsorbs C_2H_2 over CO_2 , with uptakes of 95.7 and 48.6 cm³ cm⁻³, respectively, leading to a C_2H_2/CO_2 uptake ratio of 1.97 (Figure 2a; Figure S10). Such inverse adsorption behaviors of Ce^{IV}- and Zr^{IV} -MIL-140-4F toward CO₂ and C₂H₂ are for the first time observed on two isostructural materials differing only in the composition of the metal nodes. To further investigate this behavior, we compared the analogous Ce-/Zr-UiO-66-4F materials-derived from the same metal-ligand combination under different synthetic conditions-with MIL-140 materials (Figure 2e; Figures S10-S13). The results demonstrated that only Ce^{IV}-MIL-140-4F presents the inverse CO₂/C₂H₂ adsorption behavior.

To assess the separation potential of Ce^{IV}-MIL-140-4F for CO_2/C_2H_2 mixtures, ideal adsorbed solution theory (IAST) was applied to quantitatively evaluate the separation selectivity (Figures S15 and S16). Ce^{IV}-MIL-140-4F exhibits an excellent inverse CO_2/C_2H_2 (1/2) selectivity of up to 9.5 at 298 K. At 273 K, the selectivity can reach 41.5, much higher than that of the benchmark materials, such as Tm-OH-bdc (17.5 at 298 K),^[18] CD-MOF-1 (6.6 at 298 K),^[7] Mn(bdc)(bpe) (9.0 at 273 K),^[8] and SIFSIX-3-Ni (7.7 at 298 K).^[1d] High separation selectivity was also observed in Ce^{IV}-MIL-140-4F for CO_2/C_2H_2 (1/1) mixture, indicating promising separation potential for CO_2/C_2H_2 mixtures (Figure 2c). The high separation selectivity for CO₂/C₂H₂ mixtures accompanied with high CO₂ volumetric capacity suggest Ce^{IV}-MIL-140-4F as a new benchmark for inverse CO₂/C₂H₂ separation. Furthermore, the coverage-dependent isosteric heats (Q_{st}) of adsorption for CO2 on Ce^{IV}-MIL-140-4F was calculated to be 39.5 kJ mol⁻¹ at zero coverage, remarkably higher than that of C_2H_2 (27.4 kJ mol⁻¹), presenting a stronger affinity to CO_2 over C_2H_2 (Figure S17). It is worth noting that the affinity for CO₂ is still moderate compared to other CO₂-preferential MOFs, such as Tm-OH-bdc (45.2 kJ mol⁻¹),^[18] SIFSIX-3-Ni



Figure 2. a) CO₂ and C₂H₂ isotherms of Ce^{IV}- and Zr^{IV}-MIL-140-4F collected at 298 K. b) CO₂ and C₂H₂ isotherms of Ce^{IV}-MIL-140-4F collected at different temperatures. c) Comparison of the best-performing materials for CO₂/C₂H₂ separation. d) CO₂ and C₂H₂ isotherms at 195 K and N₂ isotherm at 77 K of Ce^{IV}-MIL-140-4F. e) CO₂ and C₂H₂ uptakes of different materials at 298 K.

 $(50.9 \text{ kJ mol}^{-1})$,^[1d] and CD-MOF-2 $(67.2 \text{ kJ mol}^{-1})$.^[7] Such a low Q_{st} value suggests facile regeneration of Ce^{IV}-MIL-140-4F under mild conditions in the CO₂/C₂H₂ separation process.

To gain deep insights into such anomalous CO₂-preferential adsorption performance, in situ PXRD measurement was carried out on CO₂-loaded Ce^{IV}-MIL-140-4F. The resolved structure shows that CO₂ is perfectly located on site I and bound by four F atoms coming from two parallel TFBDC ligands with F····C=O distances of 2.3 and 3.3 Å, respectively, indicating strong host-guest interactions (Figure 3 a-c). Notably, the distance between two F atoms from two ligands in Figure 3c becomes 5.0 Å from the initial 4.9 Å, indicating a slight rotation of benzene rings upon CO₂ adsorption. This is consistent with the stepwise adsorption isotherms. To further investigate the host-guest interaction, in situ FTIR spectra on CO₂-loaded materials were collected (Figure 3d; Figures S20-S23). Interestingly, several new peaks at around 1000 and 1700 cm⁻¹ were observed on CO₂-loaded Ce^{IV}-MIL-140-4F in comparison with the activated and CO₂-free sample, which may be due to the strong interactions between CO2 and F atoms leading to the vibration and stretching of C-F bonds in TFBDC linker. However, in other materials such as $\mathrm{Zr}^{\mathrm{IV}}$ MIL-140-4F, Ce^{IV}-MIL-140, Ce-UiO-66-4F, and Zr^{IV}-MIL-140, no new peaks at around 1700 and 1000 cm⁻¹ could be observed (Figures S20-S23), further consolidating the specific CO₂-preferential sorption performance of Ce^{IV}-MIL-140-4F.

Additionally, two peaks at 444 and 790 cm⁻¹ disappeared upon CO₂ loading, which may be due to the strong interactions between CO₂ and the framework. In contrast, DFT calculations for C_2H_2 in Ce^{IV}-MIL-140-4F indicate that C_2H_2 is located on site II with longer \equiv C-H...F distances of 2.7-3.1 Å (Figure 3e) compared to the distances between CO_2 and the framework (2.3 Å), indicating the weaker binding affinity of the framework with C₂H₂. The special binding configurations of CO2 and C2H2 in CeIV-MIL-14-4F demonstrate the efficiency of the constructive strategy for CO2-selective sorbents. A similar binding mode for C2H2 on site II was observed in Zr^{IV}-MIL-140-4F with distances of 2.7-3.1 Å. Furthermore, the host-guest interaction between C₂H₂ and Zr^{IV}-MIL-140-4F was consolidated by the π ··· π interaction between benzene ring on TFBDC and the triple bond on C₂H₂ (3.3 Å, Figure 3 f). Similarly, CO₂ also located on site II with distances of 2.8-3.2 Å, shorter than that of C₂H₂, and no interactions between benzene rings and CO₂ were observed (Figure S24). The binding energy of Zr^{IV}-MIL-140-4F for C_2H_2 predicated by DFT calculations is 39.5 kJ mol⁻¹, higher than that of CO_2 (33.1 kJ mol⁻¹). This is consistent with the adsorption isotherms that Zr-MIL-140-4F exhibits the preferential adsorption ability for C₂H₂ over CO₂.

To evaluate the feasibility of Ce^{IV} -MIL-140-4F for selective inverse CO_2/C_2H_2 separation, transient breakthrough simulations were performed in fixed-bed adsorption processes.^[19] The results show that highly efficient separations can be



Figure 3. a) Experimental in situ and refined PXRD patterns of CO₂-loaded Ce^{IV}-MIL-140-4F. b,c) Refined structure of CO₂-loaded Ce^{IV}-MIL-140-4F with CO₂ strongly bound by four F atoms. d) In situ FTIR spectra of the activated and CO₂-loaded Ce^{IV}- and Zr^{IV}-MIL-140-4F. e) The binding site of C₂H₂ in Ce^{IV}-MIL-140-4F. f) The DFT-calculated binding configuration of C₂H₂ in Zr^{IV}-MIL-140-4F.

accomplished by Ce^{IV}-MIL-140-4F for CO₂/C₂H₂ (1/1 and 1/2) mixtures at 273 and 298 K, with high-purity C₂H₂ harvested via a one-step breakthrough experiment (Figure 4a; Figure S25a). The calculated productivity of high-purity C₂H₂ (>99%) can reach 132.2 and 66.6 m³L⁻¹ at 273 K and 298 K, respectively, much higher than that on PCP-NH₂-ipa (28.5 m³L⁻¹).^[17] We further carried out the experimental breakthrough studies with CO₂/C₂H₂ (1/1 and 1/2) mixtures flowed over a Ce^{IV}-MIL-140-4F-packed column at 273 and

298 K (Figure 4b; Figure S25b). A clear separation of CO_2/C_2H_2 mixtures was realized, which is consistent with the simulated breakthrough results. C_2H_2 eluted through the column first to yield an outflow of pure C_2H_2 (> 99.99%) with an undetectable amount of CO_2 in a single breakthrough operation. Notably, this is difficult for C_2H_2 -selective adsorbents in the desorption process due to the co-adsorption of C_2H_2 and CO_2 . Furthermore, CO_2 can be efficiently retained in the column for long periods with the dynamic capture



Figure 4. a) Simulated and b) experimental breakthrough curves for CO_2/C_2H_2 (1/1) separation in a fixed bed packed with Ce^{IV}-MIL-140-4F at 273 and 298 K. c) Simulated and experimental breakthrough curves of C_2H_2/CO_2 (1/1) mixture on Zr^{IV} -MIL-140-4F at 298 K. All the simulated and experimental breakthrough curves were investigated at 1 bar with a flow rate of 2 mLmin⁻¹.

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amounts of 136.9 and $99.7 \text{ cm}^3 \text{ cm}^{-3}$ at 273 and 298 K, respectively. Such a high working capacity is coincident with the CO_2 adsorption isotherms. Moreover, the CO_2/C_2H_2 separation performance was unimpeded by humidity (Figure S26), which may be due to the hydrophobic pore channels. The remarkable roll-up phenomenon on C₂H₂ curves indicates strong competitive sorption of CO₂ over C₂H₂ on Ce^{IV}-MIL-140-4F. The separation factors for CO_2/C_2H_2 (1/1) mixtures calculated from breakthrough experiments are 4.9 and 5.6 at 298 and 273 K, respectively. In contrast, Zr^{IV}-MIL-140-4F exhibits good separation performance for C_2H_2/CO_2 mixtures (Figure 4c). Last but not least, the cycle and regeneration capabilities of Ce^{IV}-MIL-140-4F were investigated (Figures S27 and S28). The results show that the column can be simply regenerated by purging He at room temperature. The inverse CO2/C2H2 separation capability of CeIV-MIL-140-4F was well retained with no noticeable decrease observed, confirming its good stability for inverse CO₂/C₂H₂ separation. The above results demonstrate that Ce^{IV}-MIL-140-4F can be a promising adsorbent for inverse CO_2/C_2H_2 separation with desirable high-purity C₂H₂ obtained via a single separation operation.

Conclusion

In summary, we judiciously realized the efficient inverse CO₂/C₂H₂ adsorption and separation with an ultramicroporous Ce^{IV}-based MOF, Ce^{IV}-MIL-140-4F. Owing to the unoccupied 4f orbitals of Ce^{IV} with a strong electron-withdrawing effect from the fluorinated linkers, Ce^{IV}-MIL-140-4F exhibits optimal pore chemistry of negative electrostatic potential around four F atoms coming from two parallel linkers. This optimal pore environment can preferentially trap CO_2 through the strong F···C=O interactions. On the contrary, Zr^{IV}-MIL-140-4F only shows a normal C₂H₂/CO₂ separation selectivity. The inverse CO2-selective sorption behavior of Ce^{IV}-MIL-140-4F was revealed by in situ PXRD and FTIR experiments, as well as molecular calculations. Such unique pore chemistry endows Ce^{IV}-MIL-140-4F with benchmark inverse CO_2/C_2H_2 separation performance. High-purity C_2H_2 (>99.99%) can be directly obtained from CO_2/C_2H_2 mixtures through a single adsorption procedure, which was confirmed by the detailed simulated and experimental breakthrough studies. The elaborate design strategy for pore chemistry based on the intrinsic nature or differences between molecules is an effective way to control the discrimination ability of porous materials. This work opens a new avenue for the design of advanced porous materials in gas separation.

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Conflict of Interest

The authors declare no conflict of interest.

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Supporting Information

Optimal Pore Chemistry in an Ultramicroporous Metal–Organic Framework for Benchmark Inverse CO₂/C₂H₂ Separation

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Experimental Procedures

Synthesis of Ce(IV)- and Zr(IV)-MIL-140-4F

Ce(IV)-MIL-140-4F was synthesized according to the reported method.^[1] A mixture of cerium ammonium nitrate ($(NH_4)_2Ce(NO_3)_6$, CAN, 0.548 g, 1 mmol) and tetrafluoroterephthalic acid (H_2TFBDC , 0.238 g, 1 mmol) in deionized (DI) water (50 mL) was heated to 110 °C under stirring and refluxed for 24 h. The obtained yellow solid was filtered and washed with water and acetone. The solid was then dried under vacuum at 80 °C for 24 h, resulting in Ce(IV)-MIL-140-4F. Differently, Zr(IV)-MIL-140-4F was achieved by refluxing the mixtures of zirconium tetrachloride (ZrCl₄, 0.233 g, 1 mmol) and H_2TFBDC (0.238 g, 1 mmol) in acetonitrile (50 mL) at 120 °C under stirring for 48 h. The resulted slurry was centrifuged and washed with acetone three times, then dried under vacuum at 120 °C for 24 h, leading to Zr(IV)-MIL-140-4F.

Synthesis of Ce-UiO-66-4F

Briefly, CAN (0.548 g, 1 mmol), H_2TFBDC (0.238 g, 1 mmol), and acetic acid (6 mL) were dissolved in DI water (45 mL) in a roundbottom flask. The solution was heated to 110 °C under stirring and refluxed for 24 h. The obtained yellow solid was collected and washed three times with DI water and once with acetone. The solid was then dried at 80 °C for 24 h, resulting in Ce-UiO-66-4F.

Synthesis of Zr(IV)-MIL-140

A mixture of 1,4-benzenedicarboxylic acid (H_2BDC , 0.332 g, 2 mmol), $ZrCI_4$ (0.233 g, 1 mmol), and DMF (8 mL) was gently stirred and introduced into a 25 mL Teflon-lined steel autoclave. The autoclave was sealed and placed in an oven at 220 °C and kept for 16 h. The white solid was then filtered and dried at 100 °C for 12 h, leading to Zr(IV)-MIL-140.

Synthesis of Ce(IV)-MIL-140

Briefly, CAN (0.274 g, 0.5 mmol) and H_2BDC (0.249 g, 0.75 mmol) were dissolved in acetonitrile (10 mL), then introduced into a microwave glass reactor (25 mL). The reactor was sealed and heated for 4 h at 140 °C. After cooling down to room temperature, the yellow product was filtered off, washed with acetone three times. The solid was then dried under vacuum at 100 °C for 12 h, resulting in Ce(IV)-MIL-140.

TGA measurements

Thermogravimetric analyses (TGA) were performed on TA Instruments STD-600 at a heating rate of 10 K min⁻¹ up to 800 °C with an N₂ flow rate of 50 mL min⁻¹. The sample holders were alumina crucibles, and the amount of sample used in each measurement was 10 (\pm 2) mg. The data collected were analyzed using Universal Analysis software (version 4.4A) from TA Instruments.

Gas sorption experiments

Adsorption and desorption experiments of CO_2 and C_2H_2 were performed at different temperatures on a Micromeritics ASAP 2020 instrument equipped with commercial software for data calculation and analysis. The test temperatures were controlled by soaking the sample cell into a circulating water bath (298 K) or ice water bath (273 K). Before measurement, the sample (80–100 mg) was degassed at 373 K for 12 h. The gas isotherms were obtained under a pressure range of 0–100 kPa. CO_2 and N_2 isotherms at 196 K and 77 K, respectively, were also collected on a Micromeritics ASAP2020 instrument. The measurement temperatures were maintained at 195 and 77 K using dry ice/acetone and liquid nitrogen, respectively.

Powder X-ray diffraction analyses

Powder X-ray diffraction (PXRD) patterns were collected using a Rigaku Miniflex 600 diffractometer (Cu K $\alpha \lambda$ = 1.540598 Å) with an operating power of 40 kV, 15 mA, and a scan rate of 2.0 ° min⁻¹. The data were collected in a two-theta range of 5–40°. In situ PXRD patterns were collected with a chamber holding the sample, which was firstly evacuated and then filled with CO₂ gas. Pawley refinement was performed on the obtained PXRD data using the Reflex Module in *Materials Studio* software. Due to the abundant atoms in the crystal unit cell, the ligand molecule and the gas molecule were both treated as rigid bodies during the Pawley refinements, with the molecule orientation and center of mass freely refined. Final refinement on the positions/orientations of the rigid bodies, thermal factors, occupancies, lattice parameters, background, and profiles converged with satisfactory *R*-factors.

In situ Fourier transform infrared spectroscopy

The *in situ* Fourier transform infrared (FTIR) spectra were recorded using an FTIR spectrometer (Bruker VERTEX 70-FTIR). Before each experiment, the sample (~100 mg) was pretreated under high vacuum conditions (< 3 μ mHg) at 393 K for 6 h, and then cooled to room temperature. The sample was then exposed to CO₂ with a pressure of 1.0 bar for 24 h to ensure that the adsorption has reached equilibrium. Then the sample was used for FTIR measurements. All the spectra were recorded over accumulative 32 scans with a resolution of 4 cm⁻¹ in the range of 4000–400 cm⁻¹.

Breakthrough experiments

The breakthrough experiments were performed using a home-built dynamic gas breakthrough setup. The experiment was conducted using a stainless-steel column (4.6 mm inner diameter \times 50 mm length). Before the breakthrough experiment, the column packed with Ce(IV)- or Zr(IV)-MIL-140-4F (0.55 or 0.5 g, respectively) was firstly activated with a He flow (5 mL min⁻¹) at 423 K for 12 h. After activation, the gas mixture (C₂H₂/CO₂, volume ratio of 1/1 or 2/1) was introduced, and outlet gas from the column was monitored by a

mass spectrometer (Hiden QGA quantitative gas analysis system). After the breakthrough experiment, the sample was regenerated with a He flow (5 mL min⁻¹) at 373 K. Before each cyclic experiment, the sample was activated by heating at 100 °C for 6 h.

Breakthrough simulations

Transient breakthrough simulations were performed using the simulation methodology described previously.^[2] The breakthrough experiments were conducted in a tube of diameter d = 4.6 mm and length L = 0.05 m. The mass of the crystallites in the packed tube is m_{ads} . For a crystal framework density of ρ kg m⁻³, we calculated $(1 - \varepsilon) = \frac{\frac{m_{ads}}{\rho}}{\frac{m^2 L}{4}}$ and $\varepsilon = 1 - \frac{\frac{m_{ads}}{\rho}}{\frac{m^2 L^2}{4}}$. The crystal framework densities of Ce(IV)-MIL-140-4F and Zr(IV)-MIL-140-4F are 2170 kg m⁻³ and 2050 kg m⁻³, respectively. The total flow rate of the gas mixture at the entrance $Q_0 = 2$ mL min⁻¹ = 3.333 × 10⁻⁸ m³ s⁻¹. The superficial gas velocity at the inlet to the adsorber $u = \frac{Q_0}{\frac{\pi d^2}{4}}$. The interstitial velocity

 $v = \frac{Q_0}{\epsilon \pi d^2}$. The breakthrough simulations were performed for a total gas pressure of 100 kPa, with a constant temperature of 273 or 298

K. During the initial transience, the effluent gas contains pure C_2H_2 , and this continues until CO₂ starts breaking through because its uptake capacity in the MOF has been reached. During a certain interval, τ_{break} , pure C_2H_2 can be recovered in the gas phase. The desired purity level for C_2H_2 was set at say 99%+, then the number of moles of C_2H_2 purged during the time intervals 0 to τ_{break} , can be determined from a material balance. Dividing the purged number of moles of C_2H_2 by the mass of adsorbent in the bed, m_{ads} , yields the productivity of C_2H_2 (mol kg⁻¹). The gravimetric CO₂ uptake capacity, expressed in mol kg⁻¹, can be determined from a material balance.

DFT calculations

First-principles density functional theory (DFT) calculations were performed in Castep software (*BIOVIA Materials Studio*).^[3] A semiempirical addition of dispersive forces to conventional DFT was included in the calculation to account for van der Waals interactions. Vanderbilt-type ultra-soft pseudopotentials and generalized gradient approximation with Perdew–Burke–Ernzerhof exchange correlation were used. A cutoff energy of 590 eV and a 1 × 1 × 2 *k*-point mesh (generated using the Monkhorst-Pack scheme) were found to be enough for the total energy to converge within 0.01 meV atom⁻¹. The structures of the synthesized materials were firstly optimized, then various guest gas molecules were introduced to various locations of the channel pore, followed by a full structural relaxation. To obtain the gas binding energy, an isolated gas molecule placed in a supercell (with the same cell dimensions as the material crystal) was also relaxed as a reference. The static binding energy (at *T* = 0 K) was then calculated using: $E_B = E_{(MOF)} + E_{(gas)}$ - $E_{(MOF + gas)}$.

IAST selectivity calculations

The isotherm data for CO₂ and C₂H₂ were fitted with dual-site Langmuir-Freundlich isotherm model:^[4]

$$q = q_{A,sat} \frac{b_A p^{\nu_A}}{1 + b_A p^{\nu_A}} + q_{B,sat} \frac{b_B p^{\nu_B}}{1 + b_B p^{\nu_B}}$$
(1)

With T-dependent parameters b:

$$b = b_0 \exp\left(\frac{E}{RT}\right) \tag{2}$$

The adsorption selectivity for CO_2/C_2H_2 separation is defined by:

$$S_{ads} = \frac{q_1/q_2}{p_1/p_2}$$
(3)

Where q_1 and q_2 are the molar loadings in the adsorbed phase in equilibrium with the bulk gas phase with partial pressures p_1 and p_2 .

Isosteric heat of adsorption calculations

A virial-type expression comprising the temperature-independent parameter a_i and b_j was employed to calculate the heat of adsorption for different gases (at different temperatures). In each case, the data were fitted using the equation:^[5]

$$\ln P = \ln N + 1/T \sum_{i=0}^{m} a_i N^i + \sum_{j=0}^{n} b_j N^j$$
(4)

Here, *P* is the pressure expressed in Pa, *N* is the amount adsorbed in mmol g^{-1} , *T* is the temperature in K, a_i and b_j are virial coefficients, and *m*, *n* represent the number of coefficients required to adequately describe the isotherms.

The values of the virial coefficients a_0 through a_m were then used to calculate the isosteric heat of adsorption using the following expression:

$$Q_{st} = -R \sum_{i=0}^{m} a_i N^j \tag{5}$$

 Q_{st} is the coverage-dependent isosteric heat of adsorption and R is the universal gas constant.

Supplementary Figures



Figure S3. TGA curves of various materials collected with a heating rate of 10 K min⁻¹ and an N₂ flow rate of 50 mL min⁻¹.



Figure S4. Experimental PXRD patterns of Ce(IV)-MIL-140-4F before and after disposition under various conditions.



Figure S5. CO₂ sorption isotherms on Ce(IV)-MIL-140-4F after different treatments at 298 K.







Figure S7. Pore size distributions of Ce(IV)-MIL-140-4F (a) and Zr(IV)-MIL-140-4F (b) derived from N₂ isotherms at 77 K.



Figure S8. PXRD patterns of Zr(IV)-MIL-140-4F and Zr(IV)-MIL-140.



Figure S9. PXRD patterns of activated and CO₂-loaded Ce-UiO-66-4F.



Figure S10. CO_2 and C_2H_2 adsorption isotherms of Zr(IV)-MIL-140-4F collected at 273 and 298 K.



Figure S11. CO_2 and C_2H_2 adsorption isotherms of Ce-UiO-66 collected at 273 and 298 K.



Figure S12. CO_2 and C_2H_2 adsorption isotherms of Ce-UiO-66-4F collected at 273 and 298 K.



Figure S13. CO_2 and C_2H_2 adsorption isotherms of Zr-UiO-66-4F collected at 273, 298, and 313 K.



Figure S14. CO_2 and C_2H_2 adsorption isotherms of TIFSIX-3-Ni and GeFSIX-3-Ni at 298 K.



Figure S15. IAST adsorption selectivity for equimolar C₂H₂/CO₂ mixture of Ce(IV)/Zr(IV)-MIL-140-4F, and GeFSIX-3-Ni.



Figure S16. IAST adsorption selectivity for CO_2/C_2H_2 (1/2) mixture of Ce(IV)-MIL-140-4F.



Figure S18. The virial fitting of C₂H₂ and CO₂ sorption isotherms for Ce(IV)-MIL-140-4F (a and b) and Ce-UiO-66-4F (c and d).



Figure S19. The virial fitting of C₂H₂ and CO₂ sorption isotherms for Zr(IV)-MIL-140-4F (a and b) and Zr-UiO-66-4F (c and d).



Figure S20. In situ FTIR spectra of activated and CO2-loaded Ce(IV)-MIL-140.



Figure S21. In situ FTIR spectra of activated and CO₂-loaded Ce-UiO-66-4F.



Figure S22. In situ FTIR spectra of activated and CO₂-loaded Zr(IV)-MIL-140-4F.



Figure S23. In situ FTIR spectra of activated and CO₂-loaded Zr(IV)-MIL-140.



Figure S24. DFT-calculated configuration of CO_2 in the pore channel of Zr(IV)-MIL-140-4F.



Figure S25. Simulated (a) and experimental (b) breakthrough curves for CO_2/C_2H_2 (1/2) mixture on Ce(IV)-MIL-140-4F at 273 and 298 K. **Note:** All the simulated and experimental breakthrough curves were investigated at 1 bar with a flow rate of 2 mL min⁻¹.



Figure S26. Breakthrough curves for CO_2/C_2H_2 (1/1) mixture on Ce(IV)-MIL-140-4F with 72% humidity at 298 K with a flow rate of 2 mL min⁻¹.



Figure S27. Desorption curves of C_2H_2 and CO_2 from Ce(IV)-MIL-140-4F-packed column collected by purging He with a flow rate of 10 mL min⁻¹ at 298 K.



Figure S28. Multiple-cycle breakthrough tests of Ce(IV)-MIL-140-4F for CO₂/C₂H₂ (1/1) separation at 273 K.



Figure S29. Schematic illustration of the breakthrough setup used in this study.

Supplementary Tables

	Zr(IV)-MIL-140-4F
Refinement method	Pawley
Empirical formula	ZrO5C8F4
Formula weight	243.3
Wavelength/Å	1.54056
Crystal system	monoclinic
Space group	C2/c
a (Å)	25.8173
b (Å)	11.6115
c (Å)	8.0821
β (°)	96.0813
V (Å3)	2253
Ζ	8
<i>Calc. density</i> /g cm ⁻³	2.051
$R_{ ho}$	3.3%
R _{wp}	5.4%
GOF	2.1

Table S1. Crystallographic parameters and refinement details of Zr(IV)-MIL-140-4F.

Table S2. Dual-site Langmuir-Freundlich parameter fits for CO_2 and C_2H_2 of different materials.

		Site A			Site B		
		q A,sat	bА	VA	Q B,sat	bв	VB
		mol kg⁻¹	Pa ^{-vA}		mol kg ⁻¹	Pa ^{-vB}	
Ce(IV)-MIL-140-4F	CO ₂	1.7	5.737E-05	1	1.7	1.585E-18	5.2
(273 K)	C_2H_2	1.2	6.892E-05	1	0.7	6.283E-07	1
Ce(IV)-MIL-140-4F	CO ₂	1.6	2.025E-05	1	1.2	2.104E-19	4.6
(298 K)	C_2H_2	0.35	3.904E-06	1	1.4	1.138E-05	1
GeFSIX-3-Ni	CO ₂	1.16	3	1	2.50	1.098	1
(298 K)	C_2H_2	1.54	28.99	1	1.54	28.99	1
Zr(IV)-MIL-140-4F	CO ₂	1.2	7.493E-06	1	1.2	7.493E-06	1
(298 K)	C_2H_2	5	3.744E-06	1	0.8	7.301E-05	1

Table S3. List of atomic positions for CO₂-loaded Ce(IV)-MIL-140-4F.

Atom	а	b	С	U (eq)
C1	0.21666	0.27477	0.59764	0.025
C2	0.25809	0.34506	0.61261	0.025
C3	0.29651	0.31875	0.51096	0.025
F4	0.2704	0.40359	0.75302	0.025
F5	0.18123	0.28209	0.70617	0.025
C6	0.34785	0.37146	0.54282	0.025
07	0.36536	0.3869	0.6894	0.025
O8	0.36626	0.4254	0.43171	0.025
C9	0.95614	0.4572	0.21181	0.025
C10	0.95618	0.5757	0.21091	0.025
F11	0.91256	0.6322	0.16657	0.025
F12	0.91446	0.40011	0.14508	0.025
013	0.03112	0.81314	0.17175	0.025
014	0.03222	0.21566	0.17578	0.025
Ce15	0.55918	0.51436	0.16321	0.02352
O16	0.46273	0.49221	0.58686	0.025
C17	0.71702	0.77586	0.60805	0.025
C18	0.75845	0.84615	0.62301	0.025
C19	0.79688	0.81984	0.52136	0.025
F20	0.77076	0.90468	0.76343	0.025
F21	0.68159	0.78318	0.71658	0.025
C22	0.84821	0.87255	0.55323	0.025
O23	0.86573	0.88799	0.69981	0.025
O24	0.86663	0.92649	0.44212	0.025
C25	0.45578	0.95608	0.1997	0.025
C26	0.45582	0.07461	0.2005	0.025

F27	0.4122	0.13111	0.15616	0.025
E-20	0 41 41	0 00000	0 12200	0.025
FZ0	0.4141	0.09099	0.13290	0.025
O29	0.53148	0.31427	0.18385	0.025
O30	0 53258	0 71676	0 18619	0.025
0.00	0.00200	0.04007	0.10010	0.02050
Cesi	0.00002	0.01327	0.1526	0.02352
O32	0.9631	0.9933	0.59727	0.025
C33	0 78407	0 27603	0 91898	0.025
000	0.74004	0.27000	0.01000	0.020
034	0.74264	0.34613	0.90378	0.025
C35	0.70421	0.31965	1.00552	0.025
F36	0 73033	0 4046	0 76317	0.025
F07	0.10000	0.4040	0.70017	0.020
F37	0.81949	0.28351	0.81043	0.025
C38	0.65287	0.37213	0.97348	0.025
030	0 63536	0 387/0	0 82684	0.025
000	0.00000	0.00740	0.02004	0.025
040	0.63446	0.42599	0.08771	0.025
C41	0.04458	0.45518	0.30751	0.025
C42	0 04454	0 57368	0 30801	0.025
542	0.04434	0.07000	0.00001	0.025
F43	0.08816	0.63038	0.35215	0.025
F44	0.08626	0.39828	0.37443	0.025
045	0.0606	0.01522	0.24625	0.025
043	0.9090	0.01522	0.34035	0.025
O46	0.9685	0.21774	0.34435	0.025
Ce47	0.44154	0.5141	0.35591	0.02352
049	0 52700	0 40220	0.02002	0.025
040	0.53799	0.49230	0.92902	0.025
C49	0.28371	0.7749	0.90687	0.025
C50	0 24228	0 84501	0 89167	0.025
000	0.24220	0.04050	0.00101	0.020
651	0.20385	0.81853	0.99341	0.025
F52	0.22997	0.90348	0.75106	0.025
F53	0 31913	0 78238	0 79832	0.025
054	0.01010	0.70200	0.10002	0.020
654	0.15251	0.87101	0.96137	0.025
O55	0.135	0.88637	0.81473	0.025
056	0 13/1	0 02/87	0.0756	0.025
050	0.1341	0.32407	0.0730	0.025
C57	0.54494	0.95628	0.31792	0.025
C58	0.5449	0.0748	0.32011	0.025
E50	0 58853	0 1315	0 36425	0.025
139	0.50055	0.1313	0.30423	0.025
F60	0.58662	0.89937	0.38483	0.025
O61	0.46924	0.31413	0.33594	0.025
062	0 46814	0 71661	0 33225	0.025
002	0.40014	0.71001	0.00220	0.025
Ce63	0.9419	0.01523	0.36802	0.02352
O64	0.03763	0.99125	0.91692	0.025
CGE	0 79/07	0 72744	0 /1007	0.025
005	0.70407	0.72741	0.41907	0.025
C66	0.74264	0.65712	0.4049	0.025
C67	0.70421	0.68344	0.50655	0.025
E68	0 73033	0 5086	0.26440	0.025
100	0.73033	0.5900	0.20449	0.025
F69	0.81949	0.72009	0.31134	0.025
C70	0.65287	0.63073	0.47469	0.025
071	0 63536	0 61520	0 32811	0.025
071	0.00000	0.01523	0.52011	0.025
072	0.63446	0.57679	0.5858	0.025
C73	0.04458	0.54498	0.8057	0.025
C74	0 04454	0 42648	0 8066	0.025
575	0.001101	0.12010	0.0000	0.020
F/5	0.08816	0.36998	0.85094	0.025
F76	0.08626	0.60207	0.87243	0.025
077	0 9696	0 18904	0 84576	0.025
070	0.0000	0.10004	0.04070	0.020
078	0.9685	0.78652	0.84173	0.025
Ce79	0.44154	0.48782	0.8543	0.02352
080	0 53700	0 50007	0 43065	0.025
000	0.00733	0.00001	0.43003	0.025
C81	0.28371	0.22632	0.40946	0.025
C82	0.24228	0.15603	0.39449	0.025
C83	0 20385	0 18235	0 /0615	0.025
500	0.20000	0.10200	0.40010	0.025
F84	0.22997	0.09751	0.25408	0.025
F85	0.31913	0.219	0.30093	0.025
C86	0 15251	0 12963	0 46428	0 025
007	0.405	0.1440	0.0477	0.005
087	0.135	0.1142	0.31//	0.025
088	0.1341	0.07569	0.57539	0.025
C89	0.54494	0.04611	0.81781	0.025
000	0 5 4 40	0.00750	0.04704	0.005
C90	0.0449	0.92100	0.01701	0.025
F91	0.58853	0.87108	0.86134	0.025
F92	0.58662	0.1032	0.88453	0.025
002	0.46004	0.69700	0.00000	0.025
093	0.40924	0.00/92	0.03300	0.025
094	0.46814	0.28543	0.83132	0.025
Ce95	0.9419	0.98891	0.86471	0.02352
006	0.02762	0 00000	0 42024	0.025
090	0.03/03	0.00000	0.42024	0.020

SUPPORTING INFORMATION

C97	0.21666	0.72616	0.09853	0.025
C98	0.25809	0.65605	0.11373	0.025
C99	0.29651	0.68253	0.01199	0.025
F100	0 2704	0 59758	0 25434	0.025
E101	0.18122	0.71868	0.20709	0.025
C100	0.10123	0.71000	0.20700	0.025
0102	0.34765	0.63005	0.04403	0.025
0103	0.36536	0.61469	0.19067	0.025
O104	0.36626	0.57619	0.9298	0.025
C105	0.95614	0.547	0.71	0.025
C106	0.95618	0.4285	0.7095	0.025
F107	0.91256	0.37181	0.66536	0.025
F108	0.91446	0.60391	0.64308	0.025
0109	0.03112	0 18696	0 67116	0.025
0110	0.03222	0 78445	0.67316	0.025
Ce111	0.55918	0.48808	0.6616	0.020
0112	0.46272	0.50001	0.0010	0.02002
0112	0.40273	0.00901	0.00040	0.025
0113	0.71702	0.22728	0.11063	0.025
C114	0.75845	0.15717	0.12584	0.025
C115	0.79688	0.18366	0.0241	0.025
F116	0.77076	0.0987	0.26645	0.025
F117	0.68159	0.2198	0.21919	0.025
C118	0.84821	0.13117	0.05614	0.025
O119	0.86573	0.11581	0.20278	0.025
O120	0.86663	0.07732	0.94191	0.025
C121	0 45578	0.04591	0 69959	0.025
C122	0 45582	0.92738	0 6974	0.025
F123	0 4122	0.87068	0.65325	0.025
F12/	0.41/1	0.07000	0.63267	0.020
0125	0.53148	0.10201	0.68156	0.025
0120	0.53140	0.00000	0.00130	0.025
0120	0.55256	0.26557	0.00020	0.025
Cerz/	0.05882	0.98696	0.64949	0.02352
0128	0.9631	0.01093	0.10059	0.025
C129	0	0.39589	0.2485	0.025
C130	0	0.63288	0.2481	0.025
C131	0	0.75988	0.24788	0.025
C132	0	0.26899	0.24872	0.025
C133	0.50036	0.89698	0.25891	0.025
C134	0.50036	0.134	0.26021	0.025
C135	0.50036	0.261	0.25999	0.025
C136	0.50036	0.77008	0.25912	0.025
C137	0	0 60408	0 74649	0.025
C138	0	0.36709	0.7469	0.020
C120	0	0.24000	0.7403	0.025
C140	0	0.24009	0.74711	0.025
0140	0	0.73096	0.74020	0.025
0141	0.50036	0.1052	0.7586	0.025
C142	0.50036	0.86818	0.7573	0.025
C143	0.50036	0.74118	0.75752	0.025
C144	0.50036	0.2321	0.75838	0.025
C145	0.73773	1.21098	-1.53743	0
O146	0.75418	1.28334	-1.3859	0
O147	0.72125	1.1387	-1.68902	0
C148	-0.23736	-0.29427	1.08027	0
O149	-0.21333	-0.35674	1.23348	0
-	0.00107	0.004.07	0.00007	0

Table S4. List of atomic positions for Zr(IV)-MIL-140-4F.

Atom	а	b	С	U (eq)
C1	0.21635	0.27834	0.58959	0.025
C2	0.25772	0.3493	0.6027	0.025
C3	0.29609	0.32369	0.49874	0.025
F4	0.27001	0.40799	0.74312	0.025
F5	0.18097	0.28503	0.70028	0.025
C6	0.34735	0.37726	0.52828	0.025
07	0.36484	0.39299	0.67455	0.025
O8	0.36574	0.43147	0.41597	0.025
C9	0.95477	0.47366	0.16614	0.025
C10	0.95481	0.59205	0.16548	0.025
F11	0.91125	0.64773	0.12325	0.025
F12	0.91315	0.41588	0.10113	0.025

O14 0.03218 0.21603 0.17524 0.0252 C17 0.55838 0.52376 0.46479 0.025 C17 0.62825 0.55757 0.46479 0.025 C19 0.75736 0.85876 0.58938 0.025 C19 0.75736 0.85876 0.58938 0.025 C20 0.79574 0.8315 0.46541 0.025 C23 0.8474 0.8602 0.51449 0.8605 0.025 C24 0.86449 0.90245 0.66122 0.025 0.256 C26 0.45513 0.94033 0.40264 0.025 C26 0.45517 0.08258 0.1788 0.025 C33 0.4517 0.1423 0.025 0.33182 0.353072 0.32336 0.15863 0.025 C33 0.96172 1.0039 0.5537 0.25 0.331 0.3449 0.28961 0.884 0.025 C37 0.7032 0.33178 0.97489 0.025	013	0.03108	0.81294	0.17243	0.025
Zr15 0.5838 0.52376 0.13713 0.02322 O16 0.46207 0.49992 0.56703 0.025 C18 0.71599 0.78781 0.57627 0.025 C19 0.75736 0.48547 0.025 C20 0.79574 0.83315 0.48541 0.025 C21 0.76965 0.91745 0.72898 0.025 C23 0.847 0.88672 0.51495 0.025 C24 0.86639 0.9245 0.66122 0.025 C26 0.45513 0.96324 0.17975 0.025 C27 0.45513 0.96324 0.1788 0.025 C33 0.53072 0.32336 0.15883 0.025 C34 0.13812 0.7255 0.16191 0.025 C33 0.96172 1.0039 0.5537 0.025 C34 0.12861 0.84715 0.47839 0.025 C35 0.74157 0.35892 0.87033 0.025	O14	0.03218	0.21603	0.17524	0.025
O16 0.46207 0.49992 0.56703 0.025 O17 0.62825 0.35757 0.46479 0.025 C19 0.75736 0.85876 0.58938 0.025 C20 0.79574 0.83515 0.48641 0.025 F21 0.76965 0.91745 0.7298 0.025 C23 0.847 0.84872 0.51495 0.025 C24 0.86449 0.90245 0.66122 0.025 C26 0.45513 0.96324 0.17975 0.025 C27 0.45517 0.08258 0.1788 0.025 C33 0.53072 0.32336 0.15863 0.025 C34 0.7857 0.45647 0.143 0.15046 0.02352 O34 0.53182 0.8703 0.025 C35 0.74594 0.28961 0.8844 0.025 C35 0.74294 0.28961 0.8743 0.025 C36 0.74157 0.35832 0.87033 0.025 <td< td=""><td>Zr15</td><td>0.55838</td><td>0.52376</td><td>0.13713</td><td>0.02352</td></td<>	Zr15	0.55838	0.52376	0.13713	0.02352
O17 0.62825 0.35757 0.46479 0.025 C18 0.71599 0.78781 0.57627 0.025 C20 0.79574 0.83315 0.48541 0.025 F21 0.76965 0.91745 0.7298 0.025 F22 0.68062 0.79449 0.68695 0.025 C23 0.847 0.88672 0.51495 0.025 C26 0.45513 0.96324 0.17975 0.025 C27 0.45517 0.08288 0.1788 0.025 C30 0.53072 0.32336 0.15883 0.025 C31 0.53182 0.7255 0.16191 0.025 C33 0.96172 1.00939 0.5537 0.025 C34 0.12861 0.844 0.025 C35 0.74928 0.41712 0.73055 0.025 C36 0.74157 0.35892 0.8793 0.025 C37 0.7325 0.33178 0.97489 0.025	O16	0.46207	0.49992	0.56703	0.025
C18 0.75736 0.85876 0.57627 0.025 C19 0.75736 0.85876 0.58938 0.025 C20 0.79574 0.83315 0.48541 0.025 F21 0.68062 0.79449 0.68695 0.025 C23 0.847 0.88672 0.51495 0.025 C24 0.86539 0.94093 0.40264 0.025 C26 0.45517 0.08258 0.1788 0.025 C26 0.45517 0.90245 0.1683 0.025 C30 0.53072 0.3236 0.1583 0.025 C31 0.53182 0.7255 0.16191 0.025 C33 0.96172 1.0039 0.5537 0.025 C35 0.78294 0.28961 0.844 0.025 C37 0.7032 0.33178 0.97489 0.025 C37 0.7032 0.33178 0.97489 0.025 C37 0.7032 0.33178 0.97489 0.025 <td>017</td> <td>0.62825</td> <td>0.35757</td> <td>0.46479</td> <td>0.025</td>	017	0.62825	0.35757	0.46479	0.025
C19 0.75736 0.85876 0.58938 0.025 C20 0.79574 0.83315 0.48541 0.025 F21 0.68062 0.79449 0.68695 0.025 C23 0.847 0.88672 0.51495 0.025 O24 0.86449 0.90245 0.66122 0.025 O25 0.86539 0.94093 0.40264 0.025 C26 0.45513 0.96324 0.17975 0.025 C27 0.45517 0.08258 0.1788 0.025 C30 0.53072 0.32336 0.15883 0.025 C31 0.53182 0.7255 0.16191 0.025 C33 0.96172 1.00939 0.5537 0.025 C34 0.12861 0.844 0.025 0.3178 0.97489 0.025 C37 0.7032 0.33178 0.97489 0.025 C37 0.7032 0.33178 0.97489 0.025 C43 0.4154 0.39835 0.	C18	0.71599	0.78781	0.57627	0.025
C20 0.79574 0.83315 0.48541 0.025 F21 0.68062 0.79449 0.68695 0.025 C23 0.847 0.88672 0.51495 0.025 C24 0.86439 0.90245 0.66122 0.025 C25 0.86539 0.4093 0.40264 0.025 C26 0.45513 0.96324 0.13658 0.025 F28 0.41161 0.13826 0.1788 0.025 C31 0.53072 0.32336 0.15883 0.025 C33 0.96172 1.00399 0.5537 0.025 C34 0.12861 0.84715 0.47839 0.025 C35 0.78294 0.28961 0.884 0.025 C36 0.74157 0.35832 0.87033 0.025 C37 0.7332 0.33178 0.97489 0.025 C36 0.74157 0.35835 0.79911 0.025 C44 0.63355 0.4368 0.05746 0.02	C19	0.75736	0.85876	0.58938	0.025
F21 0.76965 0.91745 0.7298 0.025 F22 0.68062 0.79449 0.68695 0.025 C23 0.847 0.88672 0.51495 0.025 C24 0.86539 0.94093 0.40264 0.025 C25 0.86539 0.94093 0.40264 0.025 C26 0.45517 0.08258 0.1788 0.025 C27 0.45517 0.08258 0.18683 0.025 C33 0.53072 0.32336 0.15883 0.025 C31 0.53182 0.7255 0.16191 0.025 C33 0.96172 1.00939 0.5537 0.025 C34 0.12861 0.84715 0.4789 0.025 C35 0.78294 0.28961 0.884 0.025 C36 0.74157 0.35892 0.87933 0.025 C37 0.732 0.33181 0.94538 0.025 C36 0.74157 0.35892 0.3903 0.025 </td <td>C20</td> <td>0.79574</td> <td>0.83315</td> <td>0.48541</td> <td>0.025</td>	C20	0.79574	0.83315	0.48541	0.025
F22 0.68062 0.79449 0.68695 0.025 C23 0.847 0.88672 0.51495 0.025 C25 0.86539 0.94093 0.40264 0.025 C26 0.45513 0.96324 0.17975 0.025 C27 0.45517 0.08258 0.1788 0.025 C28 0.41161 0.13826 0.13868 0.025 C30 0.53072 0.32336 0.15883 0.025 C31 0.53182 0.7255 0.16191 0.025 C33 0.96172 1.00939 0.5537 0.025 C34 0.12861 0.84715 0.47839 0.025 C35 0.78294 0.28961 0.884 0.025 C36 0.74157 0.35832 0.8703 0.025 C37 0.7032 0.33178 0.97489 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63445 0.39835 0.79911 0.02	F21	0.76965	0.91745	0.7298	0.025
C23 0.847 0.88672 0.51495 0.025 C24 0.86539 0.94093 0.40264 0.025 C26 0.45513 0.96324 0.17975 0.025 C27 0.45517 0.08258 0.1788 0.025 F28 0.41161 0.13826 0.13658 0.025 C30 0.53072 0.32336 0.14833 0.025 C33 0.96172 1.00939 0.55377 0.025 C34 0.12861 0.84715 0.47839 0.025 C35 0.78294 0.28961 0.884 0.025 C36 0.74157 0.35892 0.87093 0.025 C37 0.7032 0.33178 0.97489 0.025 C40 0.65194 0.38331 0.94538 0.025 C43 0.72928 0.41712 0.73055 0.025 C43 0.64452 0.4555 0.3073 0.025 C44 0.65144 0.39835 0.79911 0.0	F22	0.68062	0.79449	0.68695	0.025
024 0.86449 0.90245 0.66122 0.025 025 0.86539 0.94093 0.40264 0.025 027 0.45517 0.08258 0.17975 0.025 027 0.45517 0.08258 0.13658 0.025 027 0.41351 0.00547 0.11473 0.025 030 0.53072 0.32336 0.15883 0.025 031 0.53182 0.7255 0.16191 0.0235 033 0.96172 1.00939 0.5537 0.025 033 0.96172 1.30939 0.5537 0.025 034 0.12861 0.84715 0.47839 0.025 035 0.7493 0.025 0.373 0.025 036 0.74157 0.35892 0.87093 0.025 037 0.7032 0.33178 0.97489 0.025 043 0.34452 0.45555 0.3073 0.025 044 0.5345 0.38331 0.94538 0.792	C23	0.847	0.88672	0.51495	0.025
025 0.86539 0.94093 0.40264 0.025 026 0.45517 0.096324 0.17975 0.025 F28 0.41161 0.13826 0.13658 0.025 F29 0.41351 0.90547 0.11473 0.025 O30 0.53072 0.32366 0.15883 0.025 O31 0.53182 0.7255 0.16191 0.025 O33 0.96172 1.00939 0.5537 0.025 O34 0.12861 0.84715 0.47839 0.025 C35 0.78294 0.28961 0.884 0.025 C36 0.74157 0.35892 0.87093 0.025 C37 0.7032 0.33178 0.97489 0.025 F38 0.72928 0.41712 0.73055 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63355 0.4368 0.05746 0.025 C42 0.63355 0.4368 0.37228 0	O24	0.86449	0.90245	0.66122	0.025
C26 0.45513 0.96324 0.17975 0.025 C27 0.45517 0.08258 0.1788 0.025 F28 0.41161 0.13826 0.13658 0.025 G30 0.53072 0.32336 0.15883 0.025 C33 0.53182 0.72255 0.16191 0.025 C33 0.96172 1.00939 0.5537 0.025 C34 0.12861 0.84715 0.47839 0.025 C35 0.78294 0.28961 0.884 0.025 C36 0.74157 0.35892 0.87093 0.025 C37 0.7032 0.33178 0.97489 0.025 F38 0.72928 0.41712 0.73055 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63445 0.39835 0.79911 0.025 C42 0.63355 0.3073 0.025 C44 0.4448 0.5734 0.30804 0.025 C43 </td <td>O25</td> <td>0.86539</td> <td>0.94093</td> <td>0.40264</td> <td>0.025</td>	O25	0.86539	0.94093	0.40264	0.025
C27 0.45517 0.08258 0.1788 0.025 F28 0.41161 0.13826 0.13658 0.025 F29 0.41351 0.90547 0.11473 0.025 O30 0.53072 0.32336 0.15883 0.025 O31 0.53182 0.7255 0.16191 0.025 C33 0.96172 1.00939 0.5537 0.025 C34 0.12861 0.84715 0.47839 0.025 C35 0.78294 0.28961 0.884 0.025 C37 0.7032 0.33178 0.97499 0.025 F38 0.72928 0.41712 0.73055 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63445 0.39835 0.79911 0.025 C43 0.44482 0.45555 0.3073 0.025 C44 0.04448 0.57344 0.30804 0.025 C44 0.04448 0.57346 0.29080 0.	C26	0.45513	0.96324	0.17975	0.025
F28 0.41161 0.13826 0.13658 0.025 F29 0.41351 0.90547 0.11473 0.025 O30 0.53072 0.32336 0.15883 0.025 C31 0.53182 0.7255 0.16191 0.025 C33 0.96172 1.00939 0.5537 0.025 C34 0.12861 0.84715 0.47839 0.025 C35 0.78294 0.28961 0.884 0.025 C36 0.74157 0.35892 0.87993 0.025 C37 0.7032 0.33178 0.97489 0.025 C38 0.72928 0.41712 0.73055 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63445 0.39835 0.79911 0.025 C42 0.63355 0.4368 0.05746 0.025 C43 0.04452 0.45555 0.3073 0.025 C44 0.04481 0.57344 0.30804 0.	C27	0.45517	0.08258	0.1788	0.025
F29 0.41351 0.90547 0.11473 0.025 O30 0.53072 0.32336 0.15883 0.025 O31 0.53182 0.7255 0.16191 0.025 C33 0.96172 1.00399 0.5537 0.025 C34 0.12861 0.84715 0.47839 0.025 C35 0.74294 0.28961 0.884 0.025 C36 0.74157 0.35892 0.87093 0.025 C37 0.7032 0.33178 0.97489 0.025 F38 0.72928 0.41712 0.73055 0.025 C40 0.65194 0.3831 0.94538 0.025 C41 0.63455 0.4368 0.05746 0.025 C43 0.04452 0.45555 0.3073 0.025 C44 0.63135 0.35029 0.025 F45 0.0864 0.63135 0.3024 0.025 C44 0.96711 0.23463 0.29808 0.025	F28	0.41161	0.13826	0.13658	0.025
030 0.53072 0.32336 0.15883 0.025 031 0.53182 0.7255 0.16191 0.025 2132 0.06874 0.0143 0.15046 0.02352 033 0.96172 1.00939 0.5537 0.025 034 0.12861 0.884 0.025 C35 0.74157 0.35892 0.87093 0.025 C37 0.7032 0.33178 0.97489 0.025 F38 0.72928 0.41712 0.70355 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63445 0.4368 0.05746 0.025 C43 0.04452 0.45555 0.3073 0.025 C44 0.04448 0.57394 0.30604 0.025 C44 0.08614 0.39943 0.37228 0.025 C45 0.08614 0.39943 0.3252 0.44 O4448 0.99711 0.23632 0.025 055	F29	0.41351	0.90547	0.11473	0.025
031 0.53182 0.7255 0.16191 0.025 Zr32 0.05874 0.0143 0.15046 0.02352 033 0.96172 1.00939 0.5537 0.025 C35 0.78294 0.28961 0.884 0.025 C36 0.74157 0.35892 0.87093 0.025 C37 0.7032 0.33178 0.97489 0.025 F38 0.72928 0.41712 0.73055 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63455 0.4368 0.05746 0.025 C42 0.63355 0.4368 0.05746 0.025 C43 0.04452 0.45555 0.3073 0.025 C44 0.04448 0.57394 0.3804 0.025 C44 0.04448 0.57394 0.30121 0.025 C44 0.04491 0.52142 0.33635 0.02352 C54 0.02366 0.82137 0.98849	O30	0.53072	0.32336	0.15883	0.025
Zr32 0.05874 0.0143 0.15046 0.02352 Q33 0.96172 1.00939 0.5537 0.025 C34 0.12861 0.84715 0.47839 0.025 C35 0.74157 0.35892 0.87093 0.025 C36 0.74157 0.35892 0.87093 0.025 C37 0.7032 0.33178 0.97489 0.025 F39 0.81832 0.29771 0.77333 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63455 0.4368 0.05746 0.025 C43 0.04452 0.45555 0.3073 0.025 C44 0.04448 0.57394 0.30804 0.025 C44 0.04448 0.3159 0.30121 0.025 C44 0.04691 0.52142 0.36635 0.0255 C44 0.96711 0.23463 0.29808 0.025 C54 0.20356 0.82137 0.988761	031	0.53182	0.7255	0.16191	0.025
O33 0.96172 1.00339 0.5537 0.025 O34 0.12861 0.84715 0.47839 0.025 C35 0.78294 0.28961 0.884 0.025 C37 0.7032 0.33178 0.97489 0.025 F38 0.72928 0.41712 0.73055 0.025 F39 0.81832 0.29771 0.77333 0.025 C40 0.66194 0.38331 0.94538 0.025 C41 0.63455 0.39835 0.79911 0.025 C44 0.04445 0.39835 0.79911 0.025 C44 0.63355 0.4368 0.05746 0.025 C44 0.04448 0.57394 0.30804 0.025 C44 0.04448 0.57394 0.30804 0.025 C44 0.04448 0.57394 0.30804 0.025 C44 0.044491 0.52142 0.3635 0.025 C55 0.29069 0.025 C53 0.2419	Zr32	0.05874	0.0143	0.15046	0.02352
034 0.12861 0.84715 0.47839 0.025 C35 0.78294 0.28961 0.884 0.025 C36 0.74157 0.35892 0.87093 0.025 C37 0.7032 0.33178 0.97489 0.025 F38 0.72928 0.41712 0.73055 0.025 C40 0.65194 0.38331 0.94538 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63455 0.4368 0.05746 0.025 C43 0.04452 0.45555 0.3073 0.025 C44 0.04448 0.57394 0.30804 0.025 F46 0.08614 0.39943 0.37228 0.025 C44 0.96711 0.23463 0.29808 0.025 C51 0.37104 0.35245 0.0086 0.025 C52 0.2833 0.7792 0.89761 0.025 C53 0.24193 0.84851 0.88454 0.0	033	0.96172	1.00939	0.5537	0.025
C35 0.78294 0.28961 0.884 0.025 C36 0.74157 0.35892 0.87093 0.025 F38 0.7292 0.41712 0.7333 0.025 F39 0.81832 0.29771 0.77333 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63445 0.39835 0.79911 0.025 C42 0.63455 0.4368 0.05746 0.025 C43 0.04452 0.45555 0.3073 0.025 C44 0.04448 0.57394 0.30804 0.025 C44 0.04448 0.57394 0.30804 0.025 C44 0.04448 0.57394 0.30804 0.025 C44 0.06614 0.39943 0.37228 0.025 C44 0.96821 0.83159 0.30121 0.025 C44 0.96814 0.39245 0.0086 0.025 C55 0.22904 0.90671 0.74415 0.	034	0.12861	0.84715	0.47839	0.025
C36 0.74157 0.35892 0.87093 0.025 C37 0.7032 0.33178 0.97489 0.025 F38 0.72928 0.41712 0.73055 0.025 F39 0.81832 0.29771 0.77333 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63445 0.39835 0.79911 0.025 C43 0.04452 0.45555 0.3073 0.025 C44 0.04448 0.57394 0.30804 0.025 F45 0.08804 0.63135 0.35029 0.025 C44 0.04448 0.57394 0.30804 0.025 C44 0.04448 0.57394 0.30635 0.0255 C44 0.966711 0.23463 0.29808 0.025 C54 0.37120 0.35245 0.0066 0.025 C55 0.22864 0.90671 0.74415 0.025 C56 0.31867 0.7873 0.78693 <	C35	0 78294	0 28961	0.884	0.025
C37 0.7032 0.33178 0.97489 0.025 F38 0.72928 0.41712 0.73055 0.025 F39 0.81832 0.29771 0.77333 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63455 0.4368 0.05746 0.025 C42 0.63355 0.4368 0.05746 0.025 C44 0.04442 0.43555 0.3073 0.025 C44 0.04448 0.57394 0.30804 0.025 F46 0.08614 0.39943 0.37228 0.025 C44 0.04448 0.57394 0.30804 0.025 C44 0.96821 0.83159 0.3121 0.025 C44 0.96821 0.83635 0.02352 0.50 C47 0.96821 0.8363 0.29808 0.025 C54 0.2036 0.82137 0.89861 0.025 C55 0.22964 0.90671 0.74415 0.0	C36	0 74157	0.35892	0.87093	0.025
C1.002 C1.011 C1.012 C1.011 C1.025 C1.025 F39 0.81832 0.29771 0.77333 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63445 0.39835 0.79911 0.025 C42 0.63355 0.4368 0.05746 0.025 C43 0.04452 0.45555 0.3073 0.025 C44 0.04448 0.57394 0.30804 0.025 F45 0.08804 0.63135 0.35029 0.025 C44 0.04448 0.37228 0.025 0.025 C44 0.96821 0.83159 0.30121 0.025 C44 0.966711 0.23463 0.29808 0.025 C50 0.53722 0.50142 0.30635 0.02352 O51 0.37104 0.35245 0.0086 0.025 C52 0.2833 0.7792 0.89761 0.025 C55 0.22964 0.90671 <td< td=""><td>C37</td><td>0.7032</td><td>0.33178</td><td>0 97489</td><td>0.025</td></td<>	C37	0.7032	0.33178	0 97489	0.025
Construct Construct Construct Construct Construct F39 0.81832 0.29771 0.77333 0.025 C40 0.65194 0.38331 0.94538 0.025 C41 0.63445 0.39835 0.79911 0.025 C42 0.63355 0.4368 0.05746 0.025 C44 0.04448 0.57394 0.30804 0.025 C44 0.08614 0.39943 0.37228 0.025 C44 0.966211 0.23463 0.29808 0.025 C54 0.96621 0.33635 0.0255 0.51 0.37104 0.35245 0.0086 0.025 C55 0.22964 0.90671 0.74415 0.025 0.55 0.22964 0.90671 0.74415 0.025 <t< td=""><td>E38</td><td>0.72928</td><td>0 41712</td><td>0.73055</td><td>0.025</td></t<>	E38	0.72928	0 41712	0.73055	0.025
C40 0.6194 0.3831 0.94538 0.025 O41 0.63445 0.39835 0.79911 0.025 O42 0.63355 0.4368 0.05746 0.025 C43 0.04452 0.45555 0.3073 0.025 C44 0.04448 0.57394 0.30804 0.025 F45 0.08804 0.63135 0.35029 0.025 F46 0.08614 0.39943 0.37228 0.025 O47 0.96821 0.83159 0.30121 0.025 C49 0.44091 0.52142 0.33635 0.0255 C50 0.53722 0.50142 0.90669 0.025 C51 0.37104 0.35245 0.0086 0.025 C53 0.24193 0.84851 0.88454 0.025 C54 0.20356 0.82137 0.98849 0.025 C55 0.229064 0.90671 0.74415 0.025 C55 0.13867 0.7873 0.78693 <td< td=""><td>F30</td><td>0.81832</td><td>0.29771</td><td>0.77333</td><td>0.025</td></td<>	F30	0.81832	0.29771	0.77333	0.025
Ort 0.50145 0.50301 0.74001 0.025 O41 0.63355 0.4368 0.05746 0.025 C43 0.04452 0.45555 0.3073 0.025 C44 0.04448 0.57394 0.30804 0.025 F45 0.08804 0.63135 0.35029 0.025 F46 0.06614 0.39943 0.37228 0.025 O47 0.96821 0.83159 0.30121 0.025 O48 0.96711 0.23463 0.29808 0.025 O50 0.53722 0.50142 0.30669 0.025 O51 0.37104 0.35245 0.0086 0.025 C52 0.2833 0.7792 0.89761 0.025 C53 0.24193 0.84851 0.84854 0.025 C54 0.20356 0.82137 0.98849 0.025 C55 0.22964 0.90671 0.74415 0.025 C56 0.31867 0.7873 0.78693 0	C40	0.65194	0.38331	0.94538	0.025
042 0.63355 0.4368 0.05746 0.025 043 0.04452 0.4368 0.05746 0.025 044 0.04448 0.57394 0.30804 0.025 044 0.08614 0.3943 0.37228 0.025 046 0.08614 0.3943 0.37228 0.025 047 0.96821 0.83159 0.30121 0.025 048 0.96711 0.23463 0.29808 0.025 050 0.53722 0.50142 0.90669 0.025 051 0.37104 0.35245 0.0086 0.025 052 0.2833 0.7792 0.89761 0.025 053 0.24193 0.84851 0.88454 0.025 054 0.20356 0.82137 0.98849 0.025 055 0.2290 0.8729 0.95898 0.025 055 0.2290 0.8729 0.95898 0.025 055 0.13391 0.92638 0.0716 0.025 </td <td>041</td> <td>0.63445</td> <td>0.30835</td> <td>0.34330</td> <td>0.025</td>	041	0.63445	0.30835	0.34330	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	041	0.00440	0.4368	0.05746	0.025
C43 0.10142 0.10333 0.1017 0.025 F45 0.08804 0.63135 0.35029 0.025 F46 0.08614 0.39943 0.37228 0.025 O47 0.96821 0.83159 0.30121 0.025 O47 0.96821 0.83159 0.30121 0.025 O48 0.96711 0.23463 0.29808 0.025 O50 0.53722 0.50142 0.90669 0.025 O51 0.37104 0.35245 0.0086 0.025 C52 0.2833 0.7792 0.89761 0.025 C53 0.24193 0.84851 0.88454 0.025 C54 0.20356 0.82137 0.98849 0.025 C55 0.22964 0.90671 0.74415 0.025 C56 0.31867 0.7873 0.78693 0.025 C61 0.544416 0.96502 0.29398 0.025 C61 0.544416 0.96502 0.29398 <t< td=""><td>C/3</td><td>0.00000</td><td>0.45555</td><td>0.3073</td><td>0.025</td></t<>	C/3	0.00000	0.45555	0.3073	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C43	0.04452	0.43333	0.30804	0.025
F46 0.08044 0.3943 0.37228 0.025 O47 0.96821 0.83159 0.30121 0.025 O48 0.96711 0.23463 0.29808 0.025 C49 0.44091 0.52142 0.33635 0.02352 O50 0.53722 0.50142 0.90669 0.025 O51 0.37104 0.35245 0.0086 0.025 C52 0.2833 0.7792 0.89761 0.025 C53 0.224193 0.84851 0.88454 0.025 C54 0.20356 0.82137 0.98849 0.025 C55 0.22964 0.90671 0.74415 0.025 C56 0.31867 0.7873 0.78693 0.025 C57 0.15229 0.8729 0.95898 0.025 C58 0.1348 0.88794 0.81272 0.025 C60 0.54416 0.96502 0.29398 0.025 C61 0.54412 0.08435 0.29443 0.025 C61 0.58778 0.9089 0.35895 0.025 C62 0.58778 0.9089 0.35895 0.025 C64 0.46857 0.32212 0.31454 0.025 C66 0.46747 0.72422 0.31454 0.025 C66 0.46747 0.72422 0.31454 0.025 C70 0.74157 0.69663 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 C72 0.72928 0.6	E45	0.04440	0.63135	0.35020	0.025
140 0.00014 0.83159 0.3120 0.025 047 0.96821 0.83159 0.30121 0.025 2r49 0.44091 0.52142 0.33635 0.02352 050 0.53722 0.50142 0.90669 0.025 051 0.37104 0.35245 0.0086 0.025 052 0.2833 0.7792 0.89761 0.025 053 0.24193 0.84851 0.88454 0.025 054 0.20356 0.82137 0.98849 0.025 055 0.22964 0.90671 0.74415 0.025 056 0.31867 0.7873 0.78693 0.025 057 0.1529 0.8729 0.95898 0.025 058 0.1348 0.88794 0.81272 0.025 059 0.13391 0.92638 0.07106 0.025 050 0.54416 0.96502 0.29398 0.025 061 0.544747 0.72422 0.31454 <td< td=""><td>F46</td><td>0.00004</td><td>0.00100</td><td>0.33023</td><td>0.025</td></td<>	F46	0.00004	0.00100	0.33023	0.025
O48 0.30021 0.3013 0.30121 0.3023 O48 0.96711 0.23463 0.29808 0.025 Zr49 0.44091 0.52142 0.33635 0.02352 O50 0.53722 0.50142 0.90669 0.025 C51 0.37104 0.35245 0.0086 0.025 C52 0.2833 0.7792 0.89761 0.025 C54 0.20356 0.82137 0.98849 0.025 C55 0.22964 0.90671 0.74415 0.025 C57 0.15229 0.8729 0.95898 0.025 C57 0.15229 0.8729 0.95898 0.025 C66 0.54416 0.966502 0.29398 0.025 C61 0.54412 0.08435 0.29443 0.025 C62 0.58768 0.14177 0.33669 0.025 C64 0.46857 0.32212 0.31454 0.025 C65 0.46747 0.72422 0.31168	$\cap 47$	0.00014	0.83150	0.37220	0.025
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	047	0.90021	0.03153	0.20808	0.025
Display 0.34031 0.32142 0.30033 0.025 O50 0.53722 0.50142 0.90669 0.025 C51 0.37104 0.35245 0.0086 0.025 C52 0.2833 0.7792 0.89761 0.025 C53 0.24193 0.84851 0.88454 0.025 C54 0.20356 0.82137 0.98849 0.025 F55 0.22964 0.90671 0.74415 0.025 C57 0.15229 0.8729 0.95898 0.025 C60 0.54416 0.96502 0.29398 0.025 C61 0.54416 0.96502 0.29398 0.025 C61 0.54412 0.08435 0.29443 0.025 C61 0.54416 0.96502 0.29398 0.025 C61 0.54412 0.08435 0.29443 0.025 C66 0.46857 0.32212 0.31454 0.025 C66 0.46747 0.72422 0.31168	7r/0	0.30711	0.23403	0.23635	0.023
050 0.53722 0.50142 0.90069 0.025 051 0.37104 0.35245 0.0086 0.025 C52 0.2833 0.7792 0.89761 0.025 C53 0.24193 0.84851 0.88454 0.025 C54 0.20356 0.82137 0.98849 0.025 F55 0.22964 0.90671 0.74415 0.025 C57 0.15229 0.8729 0.95898 0.025 C57 0.15229 0.8729 0.95898 0.025 C58 0.13391 0.92638 0.07106 0.025 C60 0.54416 0.96502 0.29398 0.025 C61 0.54412 0.08435 0.29443 0.025 F62 0.58578 0.9089 0.35895 0.025 C64 0.46857 0.32212 0.31454 0.025 C65 0.46747 0.72422 0.31168 0.025 C66 0.94055 0.03184 0.32275 0	050	0.44091	0.52142	0.00660	0.02352
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	050	0.33722	0.30142	0.90009	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C52	0.37104	0.35245	0.0000	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	052	0.2000	0.7792	0.09701	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C54	0.24193	0.04031	0.00434	0.025
F35 0.22304 0.30071 0.74413 0.025 F56 0.31867 0.7873 0.78693 0.025 C57 0.15229 0.8729 0.95898 0.025 O58 0.1348 0.88794 0.81272 0.025 O59 0.13391 0.92638 0.07106 0.025 C60 0.54416 0.96502 0.29398 0.025 C61 0.54412 0.08435 0.29443 0.025 C61 0.54412 0.08435 0.29443 0.025 F63 0.58578 0.9089 0.35895 0.025 C64 0.46857 0.32212 0.31454 0.025 C65 0.46747 0.72422 0.31168 0.025 C66 0.94055 0.03184 0.32275 0.02352 C67 0.03757 0.991 0.92029 0.025 C70 0.74157 0.66963 0.37089 0.025 C71 0.7032 0.69524 0.47486	CJ4 E55	0.20000	0.02137	0.90049	0.025
130 0.31007 0.1713 0.17033 0.17033 0.025 C57 0.15229 0.8729 0.95898 0.025 O58 0.1348 0.88794 0.81272 0.025 O59 0.13391 0.92638 0.07106 0.025 C60 0.54416 0.96502 0.29398 0.025 C61 0.54412 0.08435 0.29443 0.025 F62 0.58768 0.14177 0.33669 0.025 C64 0.46857 0.32212 0.31454 0.025 O65 0.46747 0.72422 0.31168 0.025 C66 0.94055 0.03184 0.32275 0.02352 O67 0.03757 0.991 0.92029 0.025 C70 0.74157 0.66963 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 C72 0.72928 0.61094 0.23047 0.025 C73 0.81832 0.73389 <td< td=""><td>F56</td><td>0.22904</td><td>0.30071</td><td>0.74413</td><td>0.025</td></td<>	F56	0.22904	0.30071	0.74413	0.025
C57 0.13223 0.8123 0.83636 0.025 O58 0.1348 0.88794 0.81272 0.025 O59 0.13391 0.92638 0.07106 0.025 C60 0.54416 0.96502 0.29398 0.025 C61 0.54412 0.08435 0.29443 0.025 F62 0.58768 0.14177 0.33669 0.025 F63 0.58578 0.9089 0.35895 0.025 O64 0.46857 0.32212 0.31454 0.025 O65 0.46747 0.72422 0.31168 0.025 C66 0.94055 0.03184 0.32275 0.02352 O67 0.03757 0.991 0.92029 0.025 C70 0.74157 0.66963 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 C72 0.72928 0.61094 0.23047 0.025 C74 0.65194 0.64167 0.44532 <td< td=""><td>C57</td><td>0.31007</td><td>0.7073</td><td>0.70093</td><td>0.025</td></td<>	C57	0.31007	0.7073	0.70093	0.025
OS8 0.1346 0.86794 0.81272 0.025 O59 0.13391 0.92638 0.07106 0.025 C60 0.54416 0.96502 0.29398 0.025 C61 0.54412 0.08435 0.29443 0.025 F62 0.58768 0.14177 0.33669 0.025 F63 0.58578 0.9089 0.35895 0.025 O64 0.466857 0.32212 0.31454 0.025 O65 0.46747 0.72422 0.31168 0.025 C66 0.94055 0.03184 0.32275 0.02352 O67 0.03757 0.991 0.92029 0.025 C69 0.78294 0.74058 0.384 0.025 C70 0.74157 0.66963 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 F73 0.81832 0.73389 0.27332 0.025 C74 0.65194 0.64167 0.44532 <td< td=""><td>050</td><td>0.13229</td><td>0.0729</td><td>0.93090</td><td>0.025</td></td<>	050	0.13229	0.0729	0.93090	0.025
C39 0.13391 0.92038 0.07106 0.025 C60 0.54416 0.96502 0.29398 0.025 C61 0.54412 0.08435 0.29443 0.025 F62 0.58768 0.14177 0.33669 0.025 C64 0.46857 0.32212 0.31454 0.025 O64 0.46857 0.32212 0.31454 0.025 O65 0.46747 0.72422 0.31454 0.025 O66 0.94055 0.03184 0.32275 0.02352 O67 0.03757 0.991 0.92029 0.025 O68 0.87068 0.86191 -0.00473 0.025 C70 0.74157 0.66963 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 F72 0.72928 0.61094 0.23047 0.025 C74 0.65194 0.64167 0.44532 0.025 O75 0.63445 0.62594 0.29905	050	0.1340	0.00794	0.01212	0.025
C60 0.54416 0.90302 0.23386 0.025 C61 0.54412 0.08435 0.29443 0.025 F62 0.58768 0.14177 0.33669 0.025 C63 0.58578 0.9089 0.35895 0.025 O64 0.46857 0.32212 0.31454 0.025 O65 0.46747 0.72422 0.31454 0.025 O66 0.46747 0.72422 0.31454 0.025 O66 0.46747 0.72422 0.31468 0.025 O66 0.46747 0.72422 0.31454 0.025 O67 0.03757 0.991 0.92029 0.025 O68 0.87068 0.86191 -0.00473 0.025 C70 0.78294 0.74058 0.384 0.025 C71 0.7032 0.69524 0.47486 0.025 C71 0.7032 0.69524 0.47486 0.025 F73 0.81832 0.73389 0.27332 0	000	0.13391	0.92030	0.07100	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C61	0.54410	0.90302	0.29390	0.025
F62 0.36768 0.14177 0.35069 0.025 F63 0.58578 0.9089 0.35895 0.025 O64 0.46857 0.32212 0.31454 0.025 O65 0.46747 0.72422 0.31168 0.025 Zr66 0.94055 0.03184 0.32275 0.02352 O67 0.03757 0.991 0.92029 0.025 O68 0.87068 0.86191 -0.00473 0.025 C69 0.78294 0.74058 0.384 0.025 C70 0.74157 0.66963 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 F72 0.72928 0.61094 0.23047 0.025 F73 0.81832 0.73389 0.27332 0.025 C74 0.65194 0.64167 0.44532 0.025 O75 0.63445 0.62594 0.29905 0.025 C77 0.04452 0.54527 0.80745 <	EGO	0.54412	0.00433	0.29445	0.025
F63 0.36378 0.9069 0.35693 0.025 O64 0.46857 0.32212 0.31454 0.025 O65 0.46747 0.72422 0.31168 0.025 Zr66 0.94055 0.03184 0.32275 0.02352 O67 0.03757 0.991 0.92029 0.025 O68 0.87068 0.86191 -0.00473 0.025 C69 0.78294 0.74058 0.384 0.025 C70 0.74157 0.66963 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 F72 0.72928 0.61094 0.23047 0.025 C74 0.65194 0.64167 0.44532 0.025 C74 0.65194 0.64167 0.44532 0.025 O75 0.63445 0.62594 0.29905 0.025 C77 0.04452 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 <	F02 E62	0.30700	0.14177	0.33009	0.025
0.64 0.46837 0.32212 0.31434 0.025 065 0.46747 0.72422 0.31168 0.025 Zr66 0.94055 0.03184 0.32275 0.02352 067 0.03757 0.991 0.92029 0.025 068 0.87068 0.86191 -0.00473 0.025 C69 0.78294 0.74058 0.3844 0.025 C70 0.74157 0.66963 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 F72 0.72928 0.61094 0.23047 0.025 C74 0.65194 0.64167 0.44532 0.025 C74 0.65194 0.64167 0.44532 0.025 O75 0.63445 0.62594 0.29905 0.025 C77 0.04452 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 0.025 F79 0.08804 0.3712 0.85034	F03	0.36376	0.9009	0.33695	0.025
065 0.40747 0.72422 0.31166 0.025 Zr66 0.94055 0.03184 0.32275 0.02352 O67 0.03757 0.991 0.92029 0.025 O68 0.87068 0.86191 -0.00473 0.025 C69 0.78294 0.74058 0.384 0.025 C70 0.74157 0.66963 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 F72 0.72928 0.61094 0.23047 0.025 F73 0.81832 0.73389 0.27332 0.025 C74 0.65194 0.64167 0.44532 0.025 O75 0.63445 0.62594 0.29905 0.025 O76 0.63355 0.58745 0.55763 0.025 C77 0.04452 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 0.025 F79 0.08804 0.3712 0.85034 <	064	0.40007	0.32212	0.31434	0.025
2160 0.94053 0.03184 0.32273 0.02322 O67 0.03757 0.991 0.92029 0.025 O68 0.87068 0.86191 -0.00473 0.025 C69 0.78294 0.74058 0.384 0.025 C70 0.74157 0.66963 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 F72 0.72928 0.61094 0.23047 0.025 F73 0.81832 0.73389 0.27332 0.025 C74 0.65194 0.64167 0.44532 0.025 C75 0.63445 0.62594 0.29905 0.025 C77 0.04452 0.58745 0.55763 0.025 C77 0.04452 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 0.025 F79 0.08804 0.3712 0.85034 0.025 C80 0.08614 0.60304 0.87246 <	000	0.40747	0.72422	0.31100	0.025
O67 0.03757 0.991 0.92029 0.025 O68 0.87068 0.86191 -0.00473 0.025 C69 0.78294 0.74058 0.384 0.025 C70 0.74157 0.66963 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 F72 0.72928 0.61094 0.23047 0.025 F73 0.81832 0.73389 0.27332 0.025 C74 0.65194 0.64167 0.44532 0.025 O75 0.63445 0.62594 0.29905 0.025 O76 0.63355 0.58745 0.55763 0.025 C77 0.04452 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 0.025 F79 0.08804 0.3712 0.85034 0.025 F80 0.08614 0.60304 0.87246 0.025 O81 0.96821 0.20598 0.80117		0.94055	0.03164	0.32275	0.02352
0.65 0.87068 0.86191 -0.00473 0.025 C69 0.78294 0.74058 0.384 0.025 C70 0.74157 0.66963 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 F72 0.72928 0.61094 0.23047 0.025 F73 0.81832 0.73389 0.27332 0.025 C74 0.65194 0.64167 0.44532 0.025 O75 0.63445 0.62594 0.29905 0.025 O76 0.63355 0.58745 0.55763 0.025 C77 0.04452 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 0.025 F79 0.08804 0.3712 0.85034 0.025 F80 0.08614 0.60304 0.87246 0.025 O81 0.96821 0.20598 0.80117 0.025	067	0.03757	0.991	0.92029	0.025
C69 0.7294 0.74056 0.364 0.025 C70 0.74157 0.66963 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 F72 0.72928 0.61094 0.23047 0.025 F73 0.81832 0.73389 0.27332 0.025 C74 0.65194 0.64167 0.44532 0.025 O75 0.63445 0.62594 0.29905 0.025 O76 0.63355 0.58745 0.55763 0.025 C77 0.04452 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 0.025 F79 0.08804 0.3712 0.85034 0.025 F80 0.08614 0.60304 0.87246 0.025 O81 0.96821 0.20598 0.80117 0.025	000	0.07000	0.00191	-0.00473	0.025
C70 0.74137 0.60963 0.37089 0.025 C71 0.7032 0.69524 0.47486 0.025 F72 0.72928 0.61094 0.23047 0.025 F73 0.81832 0.73389 0.27332 0.025 C74 0.65194 0.64167 0.44532 0.025 O75 0.63445 0.62594 0.29905 0.025 O76 0.63355 0.58745 0.55763 0.025 C77 0.04452 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 0.025 F79 0.08804 0.3712 0.85034 0.025 F80 0.08614 0.60304 0.87246 0.025 O81 0.96821 0.20598 0.80117 0.025	C09	0.76294	0.74000	0.304	0.025
C71 0.7032 0.69324 0.47466 0.025 F72 0.72928 0.61094 0.23047 0.025 F73 0.81832 0.73389 0.27332 0.025 C74 0.65194 0.64167 0.44532 0.025 O75 0.63445 0.62594 0.29905 0.025 O76 0.63355 0.58745 0.55763 0.025 C77 0.04452 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 0.025 F79 0.08804 0.3712 0.85034 0.025 F80 0.08614 0.60304 0.87246 0.025 O81 0.96821 0.20598 0.80117 0.025	C70	0.74157	0.00903	0.37009	0.025
F72 0.72928 0.61094 0.23047 0.025 F73 0.81832 0.73389 0.27332 0.025 C74 0.65194 0.64167 0.44532 0.025 O75 0.63445 0.62594 0.29905 0.025 O76 0.63355 0.58745 0.55763 0.025 C77 0.04452 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 0.025 F79 0.08804 0.3712 0.85034 0.025 C80 0.08614 0.60304 0.87246 0.025 O81 0.96821 0.20598 0.80117 0.025 O82 0.96741 0.80290 0.70976 0.025	C/1 E72	0.7032	0.69524	0.47400	0.025
F73 0.81832 0.7389 0.27332 0.025 C74 0.65194 0.64167 0.44532 0.025 O75 0.63445 0.62594 0.29905 0.025 O76 0.63355 0.58745 0.55763 0.025 C77 0.04452 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 0.025 F79 0.08804 0.3712 0.85034 0.025 F80 0.08614 0.60304 0.87246 0.025 O81 0.96821 0.20598 0.80117 0.025	F72	0.72920	0.01094	0.23047	0.025
C74 0.05154 0.04167 0.44532 0.025 O75 0.63445 0.62594 0.29905 0.025 O76 0.63355 0.58745 0.55763 0.025 C77 0.04452 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 0.025 F79 0.08804 0.3712 0.85034 0.025 F80 0.08614 0.60304 0.87246 0.025 O81 0.96821 0.20598 0.80117 0.025	Г/З С74	0.01032	0.13389	0.21332	0.025
Ors 0.03445 0.02344 0.29905 0.025 O76 0.63355 0.58745 0.55763 0.025 C77 0.04452 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 0.025 F79 0.08804 0.3712 0.85034 0.025 F80 0.08614 0.60304 0.87246 0.025 O81 0.96821 0.20598 0.80117 0.025	075	0.00194	0.04107	0.44002	0.020
0.70 0.000000 0.000000 0.00000 <th< td=""><td>075</td><td>0.03443</td><td>0.02094</td><td>0.29900</td><td>0.025</td></th<>	075	0.03443	0.02094	0.29900	0.025
Crr 0.04492 0.54527 0.80745 0.025 C78 0.04448 0.42688 0.80812 0.025 F79 0.08804 0.3712 0.85034 0.025 F80 0.08614 0.60304 0.87246 0.025 O81 0.96821 0.20598 0.80117 0.025	010	0.03355	0.56/45	0.00745	0.025
C70 0.04446 0.42080 0.80812 0.025 F79 0.08804 0.3712 0.85034 0.025 F80 0.08614 0.60304 0.87246 0.025 O81 0.96821 0.20598 0.80117 0.025 O82 0.96821 0.20598 0.80117 0.025	071	0.04452	0.04027	0.00745	0.025
F79 0.08804 0.3712 0.85034 0.025 F80 0.08614 0.60304 0.87246 0.025 O81 0.96821 0.20598 0.80117 0.025 O82 0.96821 0.20598 0.80117 0.025		0.04448	0.42000	0.00012	0.025
Cov 0.00014 0.00304 0.87246 0.025 O81 0.96821 0.20598 0.80117 0.025 O82 0.96711 0.80290 0.70926 0.025	F/9 E00	0.00004	0.3712	0.85034	0.025
OUI U.30021 U.20330 U.80117 U.U25		0.00014	0.00304	0.01240	0.025
	082	0.96711	0.80289	0.79836	0.025

084 0.53722 0.519 0.40657 0.025 085 0.37104 0.66136 0.50881 0.025 026 0.2833 0.025 0.3763 0.025 027 0.24193 0.16016 0.38422 0.025 028 0.22964 0.10148 0.2438 0.025 0291 0.13221 0.45865 0.025 0292 0.13391 0.07799 0.57096 0.025 0293 0.13391 0.07799 0.57096 0.025 0294 0.58678 0.11445 0.85866 0.025 0585 0.54412 0.93634 0.79479 0.025 0598 0.46857 0.69557 0.81477 0.025 0100 0.94055 1.00463 0.82314 0.02352 0101 0.03757 0.09954 0.4199 0.025 0102 0.87068 0.17177 0.49521 0.025 0101 0.03757 0.09451 0.0255 0.0125 <	Zr83	0.44091	0.49517	0.83647	0.02352
085 0.37104 0.66136 0.50881 0.025 C86 0.2833 0.23112 0.39733 0.025 C87 0.24193 0.16016 0.38422 0.025 C88 0.20356 0.18578 0.48819 0.025 C88 0.22964 0.10148 0.2438 0.025 C91 0.15229 0.13221 0.45865 0.025 C93 0.13391 0.07799 0.57096 0.025 C94 0.54416 0.95668 0.79385 0.025 C95 0.54412 0.93634 0.79479 0.025 F96 0.58768 0.88066 0.83702 0.025 C100 0.94055 1.00463 0.82314 0.02352 C101 0.03757 0.00954 0.4199 0.025 C103 0.29609 0.68714 -0.0216 0.025 C104 0.27772 0.66 0.10266 0.025 C105 0.29609 0.68714 -0.00129	084	0.53722	0.519	0.40657	0.025
C86 0.2833 0.23112 0.39733 0.025 C87 0.24193 0.16016 0.38422 0.025 C88 0.20356 0.18578 0.48819 0.025 C89 0.22964 0.10148 0.24438 0.28665 0.025 C91 0.15229 0.13221 0.45865 0.025 C92 0.1348 0.11647 0.31238 0.025 C93 0.1331 0.0799 0.57096 0.025 C94 0.54412 0.93634 0.79479 0.025 C95 0.5476 0.81857 0.81477 0.025 C98 0.46857 0.69557 0.81477 0.025 C100 0.4055 1.00463 0.82314 0.02352 C1010 0.3757 0.00954 0.4199 0.025 C102 0.8708 0.72142 0.20027 0.025 C103 0.21635 0.72331 0.8959 0.025 C104 0.25772 0.666 <td< td=""><td>O85</td><td>0.37104</td><td>0.66136</td><td>0.50881</td><td>0.025</td></td<>	O85	0.37104	0.66136	0.50881	0.025
Car 0.24193 0.16016 0.36422 0.023 Car 0.20366 0.18578 0.48819 0.025 F90 0.31867 0.22443 0.24665 0.025 C91 0.15229 0.13221 0.45665 0.025 C92 0.1348 0.11647 0.31238 0.025 C93 0.13391 0.07799 0.57096 0.025 C34 0.5416 0.05568 0.79385 0.025 C95 0.54412 0.93634 0.79479 0.025 C96 0.58768 0.88066 0.83702 0.025 C99 0.46747 0.29343 0.81169 0.025 C100 0.94055 1.00463 0.82314 0.02352 C101 0.03757 0.0954 0.4199 0.025 C103 0.21635 0.72931 0.08959 0.025 C104 0.27001 0.6018 0.24305 0.025 C104 0.27001 0.6018 0.24305	C86	0.2833	0.23112	0.39733	0.025
Case 0.22964 0.101876 0.48619 0.025 F89 0.22964 0.10148 0.24438 0.025 C91 0.15229 0.13221 0.45865 0.025 C92 0.1348 0.11647 0.31238 0.025 C93 0.13391 0.07799 0.57096 0.025 C94 0.54416 0.05568 0.79385 0.025 C95 0.54412 0.93634 0.79479 0.025 C97 0.58578 0.11345 0.85886 0.025 C98 0.46857 0.61477 0.29343 0.81477 0.025 C100 0.94055 1.00463 0.82314 0.0255 C103 0.21635 0.72931 0.08959 0.025 C103 0.21635 0.72931 0.08959 0.025 C104 0.257701 0.6018 0.24305 0.025 C104 0.27001 0.6018 0.24305 0.025 C105 0.29609 0.68714 -0.00129 0.025 <td></td> <td>0.24193</td> <td>0.16016</td> <td>0.38422</td> <td>0.025</td>		0.24193	0.16016	0.38422	0.025
103 0.22304 0.10143 0.2435 0.025 C91 0.15229 0.13221 0.45865 0.025 O92 0.1348 0.11647 0.31238 0.025 O93 0.13391 0.07799 0.57096 0.025 C94 0.54416 0.05568 0.79385 0.025 C95 0.54412 0.93634 0.79479 0.025 F96 0.58768 0.11345 0.88706 0.025 O98 0.466857 0.69557 0.81477 0.025 C100 0.94055 1.00463 0.82314 0.02352 O101 0.03757 0.00954 0.4199 0.025 C103 0.21635 0.72931 0.08959 0.025 C104 0.25772 0.66 0.10266 0.025 C103 0.21635 0.72931 0.08959 0.025 C104 0.27001 0.6018 0.24305 0.025 C105 0.29609 0.68714 -0.00129		0.20300	0.10070	0.40019	0.025
130 0.15229 0.13221 0.45665 0.025 092 0.13391 0.07799 0.57096 0.025 053 0.13391 0.07799 0.57096 0.025 054 0.54416 0.05568 0.79385 0.025 055 0.54412 0.93634 0.79479 0.025 056 0.58768 0.88066 0.83702 0.025 059 0.46747 0.29343 0.81169 0.025 0599 0.46747 0.29343 0.81169 0.025 0101 0.3757 0.00954 0.4199 0.025 0102 0.87068 0.17177 0.49521 0.025 0102 0.87068 0.17177 0.49521 0.025 0103 0.21635 0.72931 0.08859 0.025 0104 0.25772 0.66 0.10266 0.025 0104 0.25772 0.66 0.10282 0.025 0105 0.29009 0.68714 -0.00129	F09 F00	0.22904	0.10140	0.2436	0.025
O22 0.1348 0.11447 0.31238 0.025 O33 0.13391 0.07799 0.57096 0.025 C34 0.54416 0.05568 0.79385 0.025 C35 0.54412 0.93634 0.79479 0.025 F96 0.58768 0.88066 0.83702 0.025 C99 0.46857 0.61145 0.85886 0.025 C99 0.46877 0.29343 0.81147 0.025 C100 0.94055 1.00463 0.82314 0.0255 C101 0.03757 0.00954 0.4199 0.025 C102 0.87068 0.17177 0.49521 0.025 C103 0.21635 0.72931 0.08959 0.025 C104 0.2577001 0.6018 0.24305 0.025 C105 0.29609 0.68714 -0.00129 0.025 C106 0.27001 0.6018 0.24305 0.025 C108 0.34735 0.63561 0.02822	C91	0.15229	0.13221	0.45865	0.025
033 0.13391 0.07799 0.57096 0.025 C94 0.54416 0.05668 0.79385 0.025 C95 0.54412 0.93634 0.79479 0.025 F96 0.58578 0.11345 0.85868 0.025 O98 0.46857 0.69557 0.81477 0.0255 C998 0.46857 0.09954 0.4199 0.0255 C101 0.03757 0.00954 0.4199 0.025 C103 0.21635 0.72931 0.08959 0.025 C104 0.25772 0.66 0.10266 0.025 C105 0.28069 0.68714 -0.00129 0.025 F107 0.18097 0.72122 0.20027 0.025 C108 0.34735 0.63561 0.0282 0.025 C110 0.36574 0.58213 0.91613 0.025 C111 0.94841 0.44499 0.66556 0.025 C112 0.95481 0.44449 0.66556	092	0.1348	0.11647	0.31238	0.025
C94 0.54416 0.05568 0.79385 0.025 C95 0.54768 0.88066 0.83702 0.025 F96 0.58768 0.11345 0.85786 0.025 O98 0.46857 0.69557 0.81477 0.025 O99 0.46747 0.29343 0.81169 0.025 C100 0.94055 1.00463 0.82314 0.02352 C101 0.03757 0.00954 0.4199 0.025 C103 0.21635 0.72931 0.08959 0.025 C104 0.25772 0.66 0.10266 0.025 C104 0.25772 0.66 0.10266 0.025 C104 0.25772 0.66 0.0225 0.025 C104 0.25772 0.66 0.0225 0.025 C104 0.25772 0.66 0.0225 0.025 C108 0.34735 0.63561 0.0225 0.1025 C110 0.36574 0.58213 0.91613 0.	O93	0.13391	0.07799	0.57096	0.025
C95 0.54412 0.93634 0.79479 0.025 F96 0.58768 0.81066 0.83702 0.025 O98 0.46857 0.69557 0.81477 0.025 O99 0.46747 0.29343 0.81169 0.0255 Zr100 0.94055 1.00463 0.82314 0.02352 O101 0.03757 0.00954 0.4199 0.025 C103 0.21635 0.72931 0.08959 0.025 C104 0.25770 0.66 0.10266 0.025 C105 0.29609 0.68714 -0.00129 0.025 F106 0.27001 0.6018 0.24305 0.025 O110 0.36574 0.58213 0.91613 0.025 O110 0.36574 0.58213 0.91613 0.025 C111 0.95477 0.56337 0.66526 0.025 C112 0.95481 0.44499 0.66556 0.025 C111 0.91125 0.38757 0.62321 </td <td>C94</td> <td>0.54416</td> <td>0.05568</td> <td>0.79385</td> <td>0.025</td>	C94	0.54416	0.05568	0.79385	0.025
F96 0.58768 0.11345 0.85886 0.025 F97 0.58578 0.11345 0.85886 0.025 O99 0.46677 0.29343 0.81169 0.0255 C100 0.94055 1.00463 0.82314 0.02352 C101 0.03757 0.00954 0.4199 0.025 C103 0.21635 0.72931 0.08959 0.025 C104 0.25772 0.66 0.10266 0.025 C105 0.24609 0.68714 -0.00129 0.025 F106 0.27001 0.6018 0.24305 0.025 C108 0.34735 0.63561 0.02822 0.025 C110 0.36574 0.58213 0.91613 0.025 C111 0.95481 0.44499 0.66556 0.025 C112 0.95481 0.44499 0.67552 0.025 C114 0.91315 0.61949 0.60131 0.025 C114 0.91315 0.61949 0.6025 <td>C95</td> <td>0.54412</td> <td>0.93634</td> <td>0.79479</td> <td>0.025</td>	C95	0.54412	0.93634	0.79479	0.025
F97 0.58578 0.11345 0.85886 0.025 O98 0.46857 0.69557 0.81477 0.025 Z1100 0.94055 1.00463 0.82314 0.02352 O101 0.03757 0.00954 0.4199 0.025 C103 0.21635 0.72931 0.49521 0.025 C104 0.25772 0.66 0.10266 0.025 C105 0.29609 0.68714 -0.00129 0.025 F106 0.2701 0.6018 0.24305 0.025 C108 0.34735 0.63661 0.02822 0.025 O110 0.36574 0.58213 0.91613 0.025 O110 0.36574 0.5837 0.66556 0.025 C112 0.95481 0.44499 0.66131 0.025 C114 0.91315 0.61949 0.60131 0.025 C114 0.91318 0.74849 0.67552 0.025 Zr117 0.55838 0.4975 0.63725 <td>F96</td> <td>0.58768</td> <td>0.88066</td> <td>0.83702</td> <td>0.025</td>	F96	0.58768	0.88066	0.83702	0.025
Og8 0.46857 0.6955 0.81477 0.025 Oy9 0.46747 0.29343 0.81169 0.025 Z1100 0.94055 1.00463 0.82314 0.02352 O101 0.03757 0.00954 0.4199 0.025 C103 0.21635 0.72931 0.08959 0.025 C104 0.25772 0.66 0.10266 0.025 C105 0.29609 0.68714 -0.00129 0.025 F106 0.27001 0.6018 0.24305 0.025 C108 0.34735 0.63561 0.02822 0.025 C110 0.36574 0.58213 0.91613 0.025 C111 0.95481 0.44499 0.66556 0.025 C112 0.95481 0.44499 0.66556 0.025 C114 0.91125 0.8775 0.63725 0.025 C114 0.91315 0.61949 0.60752 0.025 C114 0.9128 0.78429 0.67552 <td>F97</td> <td>0.58578</td> <td>0.11345</td> <td>0.85886</td> <td>0.025</td>	F97	0.58578	0.11345	0.85886	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	098	0.46857	0.69557	0.81477	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	099 7r100	0.46747	0.29343	0.81169	0.025
0101 0.3017 0.00034 0.4135 0.025 0102 0.87068 0.17177 0.49521 0.025 C103 0.21635 0.72931 0.08959 0.025 C104 0.25772 0.66 0.10266 0.025 C105 0.29609 0.68714 -0.00129 0.025 F106 0.27001 0.6018 0.24305 0.025 C108 0.34735 0.63561 0.02822 0.025 C110 0.36574 0.58213 0.91613 0.025 C111 0.95477 0.56337 0.66629 0.025 C112 0.95481 0.44499 0.66131 0.025 C114 0.91315 0.61949 0.60131 0.025 C115 0.03108 0.18734 0.67238 0.025 C114 0.91315 0.66647 0.965 0.025 C120 0.71599 0.23973 0.07599 0.025 C121 0.79574 0.19755 -0.01489 <td>O101</td> <td>0.94055</td> <td>0.00403</td> <td>0.02314</td> <td>0.02352</td>	O101	0.94055	0.00403	0.02314	0.02352
C103 0.21635 0.72931 0.08959 0.025 C104 0.25772 0.66 0.10266 0.025 C105 0.29609 0.68714 -0.00129 0.025 F106 0.27001 0.6018 0.24305 0.025 C108 0.34735 0.63561 0.02822 0.025 C108 0.34735 0.63561 0.02822 0.025 C110 0.36574 0.58213 0.91613 0.025 C111 0.95481 0.44499 0.66556 0.025 C112 0.95481 0.44499 0.66556 0.025 C114 0.91125 0.38757 0.62331 0.025 C114 0.91125 0.38757 0.62331 0.025 C116 0.03218 0.78429 0.67552 0.025 C114 0.91125 0.66647 0.9655 0.025 C120 0.71599 0.23973 0.07599 0.025 C121 0.75736 0.17042 0.89806 </td <td>0102</td> <td>0.87068</td> <td>0 17177</td> <td>0 49521</td> <td>0.025</td>	0102	0.87068	0 17177	0 49521	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C103	0.21635	0.72931	0.08959	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C104	0.25772	0.66	0.10266	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C105	0.29609	0.68714	-0.00129	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	F106	0.27001	0.6018	0.24305	0.025
C108 0.34735 0.63561 0.02822 0.025 O109 0.36484 0.62057 0.17448 0.025 O110 0.36574 0.58213 0.91613 0.025 C111 0.95481 0.44499 0.66556 0.025 C112 0.95481 0.44499 0.66556 0.025 F113 0.91125 0.38757 0.62331 0.025 O115 0.03108 0.18734 0.67552 0.025 O116 0.03218 0.78429 0.67552 0.0255 O118 0.46207 0.51751 0.06691 0.025 O119 0.62825 0.66647 0.965 0.025 C120 0.71599 0.23973 0.07599 0.025 C121 0.7576 0.17042 0.08906 0.025 C122 0.79574 0.19755 -0.01489 0.025 F123 0.76965 0.11222 0.22945 0.025 C125 0.847 0.14602 0.01462<	F107	0.18097	0.72122	0.20027	0.025
O109 0.36484 0.62057 0.17448 0.025 O110 0.36574 0.58213 0.91613 0.025 C111 0.95477 0.56337 0.66629 0.025 F113 0.91125 0.38757 0.66331 0.025 F114 0.91315 0.61949 0.66131 0.025 O115 0.03108 0.18734 0.67552 0.025 O116 0.03218 0.78429 0.67552 0.0255 O118 0.46207 0.51751 0.06691 0.025 O119 0.62825 0.66647 0.965 0.025 C120 0.71599 0.23973 0.07599 0.025 C121 0.75736 0.17042 0.08906 0.025 C122 0.79574 0.19755 -0.01489 0.025 C125 0.847 0.14602 0.01462 0.025 C124 0.68062 0.23163 0.18667 0.025 C125 0.847 0.14602 0.01462 </td <td>C108</td> <td>0.34735</td> <td>0.63561</td> <td>0.02822</td> <td>0.025</td>	C108	0.34735	0.63561	0.02822	0.025
O110 0.36574 0.56337 0.91613 0.025 C111 0.95487 0.56337 0.66629 0.025 C112 0.95481 0.44499 0.66556 0.025 F113 0.91125 0.38757 0.62331 0.025 F114 0.91315 0.61949 0.60131 0.025 O115 0.03108 0.18734 0.67238 0.025 O116 0.03218 0.78429 0.67552 0.025 Zr117 0.55838 0.4975 0.63725 0.0255 O118 0.46207 0.51751 0.06691 0.025 C120 0.71599 0.23973 0.07599 0.025 C121 0.75736 0.17042 0.08906 0.025 C122 0.79574 0.19755 -0.01489 0.025 F123 0.76965 0.11222 0.22945 0.025 C126 0.8649 0.13099 0.16088 0.025 C128 0.45131 0.05391 0.67	O109	0.36484	0.62057	0.17448	0.025
C111 0.95481 0.44499 0.66556 0.025 F113 0.91125 0.38757 0.62331 0.025 F114 0.91315 0.61949 0.60131 0.025 O115 0.03108 0.18734 0.67238 0.025 O116 0.03218 0.78429 0.67552 0.025 Zr117 0.55838 0.4975 0.63725 0.025 O118 0.46207 0.51751 0.06691 0.025 C120 0.71599 0.23973 0.07599 0.025 C121 0.75736 0.17042 0.08906 0.025 C122 0.79574 0.19755 -0.01489 0.025 C123 0.76965 0.11222 0.22945 0.025 C124 0.68649 0.13099 0	O110	0.36574	0.58213	0.91613	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C112	0.95477	0.30337	0.00029	0.025
F113 0.011315 0.61101 0.60131 0.025 0115 0.03108 0.18734 0.67238 0.025 0116 0.03218 0.78429 0.67552 0.025 2r117 0.55838 0.4975 0.63725 0.02352 0118 0.46207 0.51751 0.06691 0.025 C119 0.62825 0.66647 0.965 0.025 C120 0.71599 0.23973 0.07599 0.025 C121 0.75736 0.17042 0.08906 0.025 C122 0.79574 0.19755 -0.01489 0.025 F123 0.76965 0.1122 0.22945 0.025 C125 0.847 0.14602 0.01462 0.025 C125 0.847 0.14602 0.01462 0.025 C126 0.86449 0.13099 0.16088 0.025 C128 0.45517 0.93457 0.67962 0.025 F130 0.41161 0.87716 0.63691<	F113	0.91125	0.38757	0.62331	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	F114	0.91315	0.61949	0.60131	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O115	0.03108	0.18734	0.67238	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O116	0.03218	0.78429	0.67552	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Zr117	0.55838	0.4975	0.63725	0.02352
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0118	0.46207	0.51751	0.06691	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0119	0.62825	0.66647	0.965	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C120	0.71599	0.23973	0.07599	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C122	0.75730	0.17042	-0 01489	0.025
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	F123	0 76965	0.10700	0.22945	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	F124	0.68062	0.23163	0.18667	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C125	0.847	0.14602	0.01462	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O126	0.86449	0.13099	0.16088	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0127	0.86539	0.09254	0.90253	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C128	0.45513	0.05391	0.67962	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C129	0.45517	0.93457	0.67916	0.025
C131 0.41331 0.11003 0.61484 0.025 O132 0.53072 0.6968 0.65906 0.025 O133 0.53182 0.29471 0.66192 0.025 Zr134 0.05874 0.98709 0.65085 0.02352 O135 0.96172 0.02792 0.05331 0.025 C136 0.12861 0.15701 0.97832 0.025 C137 0 0.39552 0.25017 0.025 C138 0 0.6323 0.25024 0.025 C140 0 0.26874 0.25027 0.025 C140 0 0.26874 0.25014 0.025 C141 0.49965 0.90499 0.23684 0.025 C142 0.49965 0.14271 0.23663 0.025 C143 0.49965 0.77821 0.23681 0.025 C143 0.49965 0.77821 0.23681 0.025 C144 0.49965 0.77821 0.23681 0.0	F130	0.41161	0.87716	0.63691	0.025
0132 0.03072 0.0300 0.03000 0.03000 0133 0.53182 0.29471 0.66192 0.025 Zr134 0.05874 0.98709 0.65085 0.02352 O135 0.96172 0.02792 0.05331 0.025 C136 0.12861 0.15701 0.97832 0.025 C137 0 0.39552 0.25017 0.025 C138 0 0.6323 0.25024 0.025 C139 0 0.75918 0.25027 0.025 C140 0 0.26874 0.25014 0.025 C141 0.49965 0.90499 0.23684 0.025 C142 0.49965 0.14271 0.23663 0.025 C143 0.49965 0.77821 0.23681 0.025 C144 0.49965 0.77821 0.23681 0.025 C145 0 0.60353 0.75035 0.025 C146 0 0.36675 0.75029 0.025	0132	0.41351	0.11003	0.01404	0.025
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0132	0.53182	0.29471	0.66192	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Zr134	0.05874	0.98709	0.65085	0.02352
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O135	0.96172	0.02792	0.05331	0.025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O136	0.12861	0.15701	0.97832	0.025
C138 0 0.6323 0.25024 0.025 C139 0 0.75918 0.25027 0.025 C140 0 0.26874 0.25014 0.025 C141 0.49965 0.90499 0.23684 0.025 C142 0.49965 0.14271 0.23663 0.025 C143 0.49965 0.26959 0.23667 0.025 C144 0.49965 0.77821 0.23681 0.025 C144 0.49965 0.77821 0.23681 0.025 C145 0 0.60353 0.75035 0.025 C146 0 0.36675 0.75029 0.025	C137	0	0.39552	0.25017	0.025
C139 0 0.75918 0.25027 0.025 C140 0 0.26874 0.25014 0.025 C141 0.49965 0.90499 0.23684 0.025 C142 0.49965 0.14271 0.23663 0.025 C143 0.49965 0.26959 0.23667 0.025 C144 0.49965 0.77821 0.23681 0.025 C144 0.49965 0.77821 0.23681 0.025 C145 0 0.60353 0.75035 0.025 C146 0 0.36675 0.75029 0.025 C147 0 0.26075 0.75025 0.025	C138	0	0.6323	0.25024	0.025
C140 0 0.26874 0.25014 0.025 C141 0.49965 0.90499 0.23684 0.025 C142 0.49965 0.14271 0.23663 0.025 C143 0.49965 0.26959 0.23667 0.025 C144 0.49965 0.26959 0.23681 0.025 C144 0.49965 0.77821 0.23681 0.025 C145 0 0.60353 0.75035 0.025 C146 0 0.36675 0.75029 0.025 C147 0 0.26675 0.75029 0.025	C139	0	0.75918	0.25027	0.025
C141 0.49965 0.90499 0.23684 0.025 C142 0.49965 0.14271 0.23663 0.025 C143 0.49965 0.26959 0.23667 0.025 C144 0.49965 0.77821 0.23681 0.025 C144 0.49965 0.77821 0.23681 0.025 C145 0 0.60353 0.75035 0.025 C146 0 0.36675 0.75029 0.025 C144 0.0007 0.326875 0.025	C140	0	0.26874	0.25014	0.025
C142 0.43503 0.14271 0.23003 0.025 C143 0.49965 0.26959 0.23667 0.025 C144 0.49965 0.77821 0.23681 0.025 C145 0 0.60353 0.75035 0.025 C146 0 0.36675 0.75029 0.025 C146 0 0.36675 0.75029 0.025	C141	0.49965	0.90499	0.23663	0.025
C144 0.49965 0.77821 0.23681 0.025 C145 0 0.60353 0.75035 0.025 C146 0 0.36675 0.75029 0.025 C147 0 0.36675 0.75029 0.025	C143	0.49965	0.26959	0.23667	0.025
C145 0 0.60353 0.75035 0.025 C146 0 0.36675 0.75029 0.025 C147 0 0.36675 0.75029 0.025	C144	0.49965	0.77821	0.23681	0.025
C146 0 0.36675 0.75029 0.025	C145	0	0.60353	0.75035	0.025
C1 47 0 0.22007 0.75025 0.025	C146	0	0.36675	0.75029	0.025
0.23987 0.75025 0.025	C147	0	0.23987	0.75025	0.025
C148 0 0.7303 0.75039 0.025	C148	0	0.7303	0.75039	0.025
C149 0.49965 0.11394 0.73675 0.025	C149	0.49965	0.11394	0.73675	0.025
U150 0.49965 0.87621 0.73696 0.025	C150	0.49965	0.87621	0.73696	0.025
C151 0.49905 0.74955 0.73693 0.025 C152 0.49965 0.24072 0.73679 0.025	C151	0.49965	0.24072	0.73679	0.025

Supplementary Movie Titles

Movie S1. Development of CO₂ and C₂H₂ concentration along the length of the fixed bed of Ce(IV)-MIL-140-4F at 273 K. **Movie S2.** Development of CO₂ and C₂H₂ concentration along the length of the fixed bed of Ce(IV)-MIL-140-4F at 298 K. **Movie S3.** Development of gas phase concentration along the length of the fixed bed of Zr(IV)-MIL-140-4F at 298 K.

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