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### Gas Separation Hot Paper

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# Optimal Pore Chemistry in an Ultramicroporous Metal–Organic Framework for Benchmark Inverse  $\mathrm{CO}_2\mathrm{/C}_2\mathrm{H}_2$  Separation

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**Abstract:** Isolation of  $CO_2$  from acetylene  $(C_2H_2)$  via  $CO_2$ selective sorbents is an energy-efficient technology for  $C_2H_2$ purification, but a strategic challenge due to their similar physicochemical properties. There is still no specific methodology for constructing sorbents that preferentially trap  $CO<sub>2</sub>$ over  $C_2H_2$ . We report an effective strategy to construct optimal pore chemistry in a Ce<sup>IV</sup>-based ultramicroporous metal– organic framework  $Ce^{IV}$ -MIL-140-4F, based on charge-transfer effects, for efficient inverse  $CO_2/C_2H_2$  separation. The ligandto-metal cluster charge transfer is facilitated by  $Ce^{IV}$  with lowlying unoccupied 4f orbitals and electron-withdrawing F atoms functionalized tetrafluoroterephthalate, affording a perfect pore environment to match CO<sub>2</sub>. The exceptional CO<sub>2</sub> uptake  $(151.7 \text{ cm}^3 \text{ cm}^{-3})$  along with remarkable separation selectivities (above 40) set a new benchmark for inverse  $CO_2/C_2H_2$ separation, which is verified via simulated and experimental breakthrough experiments. The unique  $CO<sub>2</sub>$  recognition mechanism is further unveiled by in situ powder X-ray diffraction experiments, Fourier-transform infrared spectroscopy measurements, and molecular calculations.

### Introduction

Acetylene  $(C_2H_2)$  is one of the predominant precursor chemicals. It is mainly produced by partial combustion of natural gas and steam cracking of hydrocarbons, with a significant contaminant of  $CO<sub>2</sub>$  unavoidably co-generated.<sup>[1]</sup> Therefore, the separation of  $CO_2$  from  $C_2H_2$  is essential in the petrochemical industry to obtain high-purity  $C_2H_2$ . However, both  $C_2H_2$  and  $CO_2$  are non-polar. They have very similar physicochemical properties (boiling points of 189.3 and 194.7 K for  $C_2H_2$  and  $CO_2$ , respectively) and almost identical size and dimension (kinetic diameter of  $3.3 \text{ Å}$  for both gases;  $3.3 \times 3.3 \times 5.7$  Å<sup>3</sup> for C<sub>2</sub>H<sub>2</sub> and  $3.2 \times 3.3 \times 5.4$  Å<sup>3</sup> for CO<sub>2</sub>; Supporting Information, Figure S1), undoubtedly giving rise to a daunting challenge for their separation.<sup>[1a-d]</sup> The

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 $CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub>$  separation process is implemented primarily by energy-intensive approaches, such as solvent extraction and cryogenic distillation. Adsorptive separation using porous adsorbents is a promising alternative technology, which is more environmentally friendly and energy-efficient than the heat-driven processes. However, the close similarities and the strict upper compression limit of  $C_2H_2$  (2 bar) handicap the utilization of conventional porous materials, such as zeolites and carbon materials, for  $CO_2/C_2H_2$  separation.<sup>[2]</sup> Thus, the development of novel porous materials for the efficient isolation of  $CO<sub>2</sub>$  from  $C<sub>2</sub>H<sub>2</sub>$  is highly urgent yet challenging.

Metal–organic frameworks (MOFs) or porous coordination polymers (PCPs), self-assembled by inorganic metal nodes or clusters with organic ligands, have emerged as a new class of crystalline porous materials,<sup>[3]</sup> and offered a unique platform for addressing the challenges of gas separation.<sup>[4]</sup> Judicious design of the pore size/shape and pore chemistry by the modular nature of MOFs based on crystal engineering and reticular chemistry endows some MOFs with unprecedented adsorption and separation behaviors for light hydrocarbons, including  $C_2H_2/C_2H_4$ ,  $C_3H_6/C_3H_8$ , C4 olefins, etc.<sup>[4,5]</sup> The almost identical molecular size of  $CO<sub>2</sub>$  and  $C<sub>2</sub>H<sub>2</sub>$  renders it impractical and quite challenging for MOFs to discriminate them via fine-tuned pore size or shape. Numerous MOFs have been reported with substantial  $C_2H_2/CO_2$  selectivity.<sup>[1c]</sup> This is due to the ease of designing active sites in MOFs for extra interactions with guests, such as acid-base interaction and hydrogen-bonding interaction. In the context of  $C_2H_2$  and  $CO<sub>2</sub>$  separation, the acidic H atoms with positive charge in  $C_2H_2$  are capable of interacting strongly with these active sites, resulting in high  $C_2H_2/CO_2$  selectivity.<sup>[6]</sup> However, since  $CO<sub>2</sub>$  is the main contaminant in  $C<sub>2</sub>H<sub>2</sub>$  (3% and even up to 50%),<sup>[2e]</sup> CO<sub>2</sub>-selective sorbents are preferred for  $C_2H_2$ purification because they will permit the direct isolation of  $C_2H_2$  as a pure raffinate product. This will also efficiently leverage extensive industrial expertise in light-product-focused adsorptive cycles.<sup>[1c,2c]</sup> Unfortunately, MOFs exhibiting inverse  $CO_2/C_2H_2$  selectivity are rare, and within this subset of materials, the trade-off between  $CO<sub>2</sub>$  adsorption capacity and inverse  $CO_2/C_2H_2$  selectivity is still a significant barrier in prevailing materials. For example, SIFSIX-3-Ni,<sup>[1d]</sup> CD- $MOFs$ ,<sup>[7]</sup> and ionic crystals<sup>[8]</sup> with  $CO<sub>2</sub>$  uptake capacities of 98.4, 60.4, and 27 cm<sup>3</sup> cm<sup>-3</sup> only exhibit  $CO_2/C_2H_2$  (1/2) selectivity of 7.7, 6.6, and 4.8, respectively. Thus, novel MOFs with high  $CO_2$  capacity and inverse  $CO_2/C_2H_2$  separation selectivity are of paramount importance in  $C_2H_2$  purification. However, seeking strategies to construct MOFs with preferential sorption of  $CO_2$  over  $C_2H_2$  is still in its infancy.

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Notably, there is a huge difference in quadrupole moment between  $CO_2$   $(-13.4 \times 10^{-40} \text{ C} \text{m}^2)^{[9]}$  and  $C_2H_2$   $(+20.5 \times$  $10^{-40}$  Cm<sup>2</sup>, Figure S1),<sup>[2d,10]</sup> enlightening us to judiciously tune the pore chemistry with inverse electrostatic potential to leverage the quadrupole moment difference between  $CO<sub>2</sub>$ and  $C_2H_2$ , thus leading to inverse  $CO_2/C_2H_2$  separation. For this reason, the metal node in MOFs should be in a high oxidation state to withdraw the electrons from ligands, producing a more polar pore surface to recognize  $CO<sub>2</sub>$ molecules preferentially. Accordingly, the strategy combining  $Ce<sup>IV</sup>$  with unoccupied 4f orbitals and perfluorinated aromatic spacer, tetrafluoroterephthalate (TFBDC), meets such a request. Herein, we explored the framework, Ce<sup>IV</sup>-MIL-140-4F, for inverse  $CO_2/C_2H_2$  adsorption and separation, and compared its performance with the isostructural  $Zr^{IV}$ -MIL-140-4F, which is for the first time obtained and investigated. Notably, this pair of MOFs provides an interesting example of diverging sorption behaviors in isostructural frameworks, in which  $Ce^{IV}$ -MIL-140-4F exhibits excellent  $CO_2$ -preferential adsorption performance over  $C_2H_2$ , while  $Zr^{\text{IV}}$ -MIL-140-4F exhibits normal  $C_2H_2$  selectivity over  $CO_2$ .  $Ce^{IV}$ -MIL-140-4F provides an optimal pore environment to match  $CO<sub>2</sub>$ , and  $CO<sub>2</sub>$  is trapped into the pores via strong host-guest interactions by four F atoms from two linkers, which is evidenced by in situ powder X-ray diffraction (PXRD) and Fouriertransform infrared spectroscopy (FTIR) studies, as well as molecular simulations. As a result,  $Ce^{IV}$ -MIL-140-4F exhibits a superior  $CO_2$  uptake of 151.7 cm<sup>3</sup> cm<sup>-3</sup> at 273 K and excellent separation selectivities (above 40) for  $CO_2/C_2H_2$ mixtures. In addition, breakthrough experiments and simulations further confirm the excellent  $CO_2/C_2H_2$  separation performance. These results render  $Ce^{IV}$ -MIL-140-4F a new benchmark material for inverse  $CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub>$  separation, which

is highly sought in the industrial separation process but rarely seen in the current literature.

### Results and Discussion

The microcrystalline powder of  $Ce<sup>IV</sup>-MIL-140-4F$  was obtained via refluxing cerium(IV) ammonium nitrate and H<sub>2</sub>TFBDC in water at 383 K for 24 h.<sup>[11]</sup> Ce<sup>IV</sup>-MIL-140-4F crystallizes in the monoclinic C2/c space group and possesses perfluorinated one-dimensional triangular pore channels, making it highly hydrophobic (Figure S2). The  $Ce<sup>IV</sup>$  ions in  $Ce<sup>IV</sup>$ -MIL-140-4F exhibit a seven-coordination mode with three bridging  $\mu_3$ -O oxygen atoms and four oxygen atoms from the dicarboxylic ligands, forming octahedral  $CeO<sub>7</sub>$ dimers. This is distinct from the 12-connected hexanuclear  $Ce_6O_4(OH)_4(COO)_{12}$  clusters with structural hydroxy groups in the UiO-66 analogs.<sup>[11,12]</sup> The octahedra  $CeO<sub>7</sub>$  dimers are connected via the corner-sharing octahedra, leading to onedimensional (1D) inorganic chains or sub-building units running along the c axis (Figure 1a). The 1D chains are connected through six TFBDC moieties in perpendicular directions, constructing 1D triangular channels with abundant F atoms stretching into the pores with pore apertures of 3.4– 4.3 Å (Figure 1 b). This pore structure is different from that in MIL-47 with 1D lozenge-shaped channels. This is due to the different coordination number of  $Ce^{IV}$  (7) compared to  $V^{V}$ (6), and the presence of a complex "double chain" inorganic building units in  $Ce^{IV}$ -MIL-140-4F (Figure 1 a) instead of a simple chain of corner-sharing octahedra in MIL-47.[13] Bulk purity of  $Ce^{IV}$ -MIL-140-4F was established by comparing experimental PXRD patterns with those calculated from crystal data (Figure 1 e). Replacing  $Ce^{IV}$  with  $Zr^{IV}$ , the perfluorinated analog  $Zr^{IV}$ -MIL-140-4F was obtained for the



Figure 1. a) One-dimensional inorganic subunit of the metal oxide chain in MIL-140-14F. b) Illustration of the crystal structure and pore chemistry of MIL-140-4F. c,d) The Hirshfeld surface with  $d_\varepsilon$  (electrostatic potential) and binding sites in Ce<sup>IV</sup>- (c) and Zr<sup>IV</sup>-MIL-140-4F (d) (red-to-blue color indicates the high-to-low transition of electron density). e) Experimental and simulated PXRD patterns of Ce<sup>IV</sup>-MIL-140-4F. f) Experimental (black) and Pawley refined (red) PXRD patterns of Zr<sup>IV</sup>-MIL-140-4F.

first time. The unit cell parameters  $(a = 25.8173, b = 11.6115,$  $c = 8.0821$ ,  $\alpha = \gamma = 90$ ,  $\beta = 96.0813$ ) were confirmed via the Pawley refinement of the PXRD patterns in conjunction with structural of acceptable fitting metrics:  $R_{wp} = 5.4\%$  and  $R_p =$ 3.3% (Figure 1 f; Supporting Information, Table S1). The unit cell of  $Ce^{IV}$ -MIL-140-4F is relatively smaller than that of  $Zr^{IV}$ -MIL-140-4F, as a consequence of the high oxidation state of  $Ce^{IV}$  with empty 4f orbitals facilitating the formation of a compact network.[11] To investigate the chemical properties of the channels and provide clues to the structure-property relationships, we analyzed the electrostatic potential distributions based on the Hirshfeld surface with  $d_e$  on MIL-140-4F materials (Figure 1 c,d).<sup>[14]</sup> The two MIL-140-4F MOFs exhibited a particular electronic distribution on their pore surface, with two distinct electronic regions in the edges of the triangular channels, denoted as electron-rich site I (blue dotted line) and electron-poor site II (pink dotted line). It is worth noting that  $Ce^{IV}$ -MIL-140-4F exhibits a much higher electron cloud density on site I and more positive potentials on site II, compared to  $Zr^{IV}$ -MIL-140-4F. This may originate from the strong electron-withdrawing effect of  $Ce<sup>IV</sup>$  with empty and low-lying 4f orbitals facilitating ligand-to-cluster charge transfer, and this process can be accelerated by the functionalization of ligands with electron-withdrawing group $s^{[12a,c,d,15]}$  Compared with the molecular properties of  $C_2H_2$ and  $CO<sub>2</sub>$ , it is expected that these two specific and distinct sites with inverse electron potential in MIL-140-4F can well match the inverse quadrupole moments of  $C_2H_2$  and  $CO_2$ . Additionally, there is an obvious difference in pore electrostatic potential on site II between  $Ce^{IV}$ - and  $Zr^{IV}$ -MIL-140-4F, which means different host-guest interaction modes may be observed on site II for  $CO<sub>2</sub>$  and  $C<sub>2</sub>H<sub>2</sub>$  adsorption.

Guest-free MIL-140-4F materials can be readily obtained at  $100^{\circ}$ C in vacuo for 12 h, and thermogravimetric analyses demonstrated that  $Ce^{IV}$ -MIL-140-4F is thermally stable up to ca. 330 $^{\circ}$ C (Figure S3). Ce<sup>IV</sup>-MIL-140-4F is chemically robust, being unaffected by soaking in water or exposing to air for prolonged periods, and even in strong acid solutions  $(1.6 \text{ mol L}^{-1} \text{ of HNO}_3)$ , as confirmed by the PXRD patterns and  $CO<sub>2</sub>$  sorption isotherms (Figures S4 and S5). The permanent porosity of MIL-140-4F materials was confirmed by  $N_2$  sorption experiments at 77 K. They exhibit fully reversible type-I isotherms without hysteresis, which is characteristic of microporous materials with permanent microporosity (Figure S6). The Brunauer-Emmett-Teller (BET) surface area and pore volume of  $Ce^{IV}$ -MIL-140-4F were calculated to be 360  $m^2g^{-1}$  and 0.11  $cm^3g^{-1}$ , respectively, relatively larger than that of  $\rm Zr^{IV}$ -MIL-140-4F (314  $\rm m^2\, g^{-1}$  and  $0.11 \text{ cm}^3 \text{g}^{-1}$ , respectively). All the values of pore size (Figure S7), volume, and surface area of MIL-140-4F materials are smaller than those of the UiO series (Figure S6) due to the simple 1D pore systems of MIL-140.

Considering the unique pore chemistry associated with suitable pore aperture size, low-pressure  $CO<sub>2</sub>$  and  $C<sub>2</sub>H<sub>2</sub>$ sorption isotherms of  $Ce^{IV}$ - and  $Zr^{IV}$ -MIL-140-4F were collected and a marked difference in the sorption behavior for  $CO<sub>2</sub>$  and  $C<sub>2</sub>H<sub>2</sub>$  was observed (Figure 2 a). Intriguingly,  $Ce^{IV}$ -MIL-140-4F exhibits an inverse  $CO_2$ -selective sorption behavior over  $C_2H_2$ . On the contrary,  $Zr^{\text{IV}}$ -MIL-140-4F

preferentially adsorbs  $C_2H_2$  over  $CO_2$ . Due to the industrial emphasis on the volume rather than the weight of the adsorbent in stationary applications, the volumetric capacity is often a better indicator of gas uptakes.<sup>[16]</sup> The  $CO<sub>2</sub>$  uptake of  $Ce^{IV}$ -MIL-140-4F is 110.3 cm<sup>3</sup> cm<sup>-3</sup> at 298 K, much higher than that of  $C_2H_2$  (41.5 cm<sup>3</sup> cm<sup>-3</sup>), giving rise to a  $CO_2/C_2H_2$ uptake ratio of 2.66. At 273 K, CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> uptakes can reach 151.7 and 53.5  $\text{cm}^3 \text{cm}^{-3}$ , respectively (Figure 2b). The uptake of  $CO<sub>2</sub>$  at 298 K is much higher than that of the most state-of-the-art  $CO_2$ -selective materials, such as MUF-16  $(74.7 \text{ cm}^3 \text{ cm}^{-3})$ ,<sup>[2c]</sup> SIFSIX-3-Ni  $(98.4 \text{ cm}^3 \text{ cm}^{-3})$ ,<sup>[1d]</sup> PCP-NH<sub>2</sub>-ipa (93.6 cm<sup>3</sup> cm<sup>-3</sup>),<sup>[17]</sup> and CD-MOFs (60.4 cm<sup>3</sup> cm<sup>-3</sup>).<sup>[7]</sup> At 273 K, the uptake is comparable with that of the benchmark Tm-OH-bdc  $(153 \text{ cm}^3 \text{ cm}^{-3})^{[18]}$  (Figure 2c), suggesting the feasibility of  $Ce^{IV}$ -MIL-140-4F in inverse  $CO_2/C_2H_2$ separation. Notably, detailed analysis shows that the  $CO<sub>2</sub>$ isotherm of  $Ce<sup>IV</sup>$ -MIL-140-4F exhibits a stepwise-shaped profile, indicating its flexibility, which may come from the rotation of benzene rings upon  $CO_2$  sorption.<sup>[1a]</sup> The steep  $CO<sub>2</sub>$  isotherm at 273 K and the attainment of the plateau at low pressures indicate the strong affinity of the framework toward  $CO_2$ . Additionally, the 196 K isotherms of  $CO_2$  and  $C_2H_2$  further confirm the preferential adsorption performance of  $Ce^{IV}$ -MIL-140-4F for CO<sub>2</sub> over C<sub>2</sub>H<sub>2</sub> (Figure 2 d). In contrast,  $Zr^{IV}$ -MIL-140-4F preferentially adsorbs  $C_2H_2$  over CO<sub>2</sub>, with uptakes of 95.7 and 48.6 cm<sup>3</sup> cm<sup>-3</sup>, respectively, leading to a  $C_2H_2/CO_2$  uptake ratio of 1.97 (Figure 2a; Figure S10). Such inverse adsorption behaviors of  $Ce<sup>IV</sup>$ - and  $Zr^{IV}$ -MIL-140-4F toward CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> are for the first time observed on two isostructural materials differing only in the composition of the metal nodes. To further investigate this behavior, we compared the analogous Ce-/Zr-UiO-66-4F materials-derived from the same metal-ligand combination under different synthetic conditions-with MIL-140 materials (Figure 2 e; Figures S10–S13). The results demonstrated that only  $Ce^{IV}$ -MIL-140-4F presents the inverse  $CO_2/C_2H_2$  adsorption behavior.

To assess the separation potential of  $Ce^{IV}$ -MIL-140-4F for  $CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub>$  mixtures, ideal adsorbed solution theory (IAST) was applied to quantitatively evaluate the separation selectivity (Figures S15 and S16).  $Ce^{IV}$ -MIL-140-4F exhibits an excellent inverse  $CO_2/C_2H_2$  (1/2) selectivity of up to 9.5 at 298 K. At 273 K, the selectivity can reach 41.5, much higher than that of the benchmark materials, such as Tm-OH-bdc  $(17.5 \text{ at } 298 \text{ K})$ ,<sup>[18]</sup> CD-MOF-1  $(6.6 \text{ at } 298 \text{ K})$ ,<sup>[7]</sup> Mn(bdc)(bpe)  $(9.0$  at 273 K),<sup>[8]</sup> and SIFSIX-3-Ni (7.7 at 298 K).<sup>[1d]</sup> High separation selectivity was also observed in  $Ce<sup>IV</sup>$ -MIL-140-4F for  $CO_2/C_2H_2$  (1/1) mixture, indicating promising separation potential for  $CO_2/C_2H_2$  mixtures (Figure 2c). The high separation selectivity for  $CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub>$  mixtures accompanied with high  $CO<sub>2</sub>$  volumetric capacity suggest  $Ce<sup>IV</sup>$ -MIL-140-4F as a new benchmark for inverse  $CO_2/C_2H_2$  separation. Furthermore, the coverage-dependent isosteric heats  $(Q_{st})$ of adsorption for  $CO_2$  on  $Ce^{IV}$ -MIL-140-4F was calculated to be 39.5  $kJ$  mol<sup>-1</sup> at zero coverage, remarkably higher than that of  $C_2H_2$  (27.4 kJ mol<sup>-1</sup>), presenting a stronger affinity to  $CO_2$ over  $C_2H_2$  (Figure S17). It is worth noting that the affinity for  $CO<sub>2</sub>$  is still moderate compared to other  $CO<sub>2</sub>$ -preferential MOFs, such as  $Tm-OH-bdc$  (45.2 kJ mol<sup>-1</sup>),<sup>[18]</sup> SIFSIX-3-Ni



**Figure 2.** a) CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> isotherms of Ce<sup>IV</sup>- and Zr<sup>IV</sup>-MIL-140-4F collected at 298 K. b) CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> isotherms of Ce<sup>IV</sup>-MIL-140-4F collected at different temperatures. c) Comparison of the best-performing materials for CO $_2$ /C $_2$ H $_2$  separation. d) CO $_2$  and C $_2$ H $_2$  isotherms at 195 K and N $_2$ isotherm at 77 K of Ce<sup>IV</sup>-MIL-140-4F. e) CO $_2$  and C $_2$ H $_2$  uptakes of different materials at 298 K.

 $(50.9 \text{ kJ} \text{ mol}^{-1})$ ,<sup>[1d]</sup> and CD-MOF-2  $(67.2 \text{ kJ} \text{ mol}^{-1})$ .<sup>[7]</sup> Such a low  $Q_{st}$  value suggests facile regeneration of Ce<sup>IV</sup>-MIL-140-4F under mild conditions in the  $CO_2/C_2H_2$  separation process.

To gain deep insights into such anomalous  $CO<sub>2</sub>$ -preferential adsorption performance, in situ PXRD measurement was carried out on  $CO_2$ -loaded  $Ce^{IV}$ -MIL-140-4F. The resolved structure shows that  $CO<sub>2</sub>$  is perfectly located on site I and bound by four F atoms coming from two parallel TFBDC ligands with F···C=O distances of 2.3 and 3.3 Å, respectively, indicating strong host-guest interactions (Figure 3 a–c). Notably, the distance between two F atoms from two ligands in Figure 3c becomes 5.0 Å from the initial 4.9 Å, indicating a slight rotation of benzene rings upon  $CO<sub>2</sub>$  adsorption. This is consistent with the stepwise adsorption isotherms. To further investigate the host-guest interaction, in situ FTIR spectra on  $CO<sub>2</sub>$ -loaded materials were collected (Figure 3d; Figures S20–S23). Interestingly, several new peaks at around 1000 and  $1700 \text{ cm}^{-1}$  were observed on  $CO_2$ -loaded  $Ce^{IV}$ -MIL-140- $4F$  in comparison with the activated and  $CO<sub>2</sub>$ -free sample, which may be due to the strong interactions between  $CO<sub>2</sub>$  and F atoms leading to the vibration and stretching of C-F bonds in TFBDC linker. However, in other materials such as  $Zr^{IV}$ -MIL-140-4F,  $Ce^{IV}$ -MIL-140, Ce-UiO-66-4F, and  $Zr^{IV}$ -MIL-140, no new peaks at around 1700 and  $1000 \text{ cm}^{-1}$  could be observed (Figures S20–S23), further consolidating the specific  $CO_2$ -preferential sorption performance of  $Ce^{IV}$ -MIL-140-4F.

Additionally, two peaks at  $444$  and  $790 \text{ cm}^{-1}$  disappeared upon  $CO<sub>2</sub>$  loading, which may be due to the strong interactions between  $CO<sub>2</sub>$  and the framework. In contrast, DFT calculations for  $C_2H_2$  in Ce<sup>IV</sup>-MIL-140-4F indicate that  $C_2H_2$  is located on site II with longer  $\equiv$ C $-H \cdot \cdot$ F distances of 2.7–3.1 Å (Figure 3 $e$ ) compared to the distances between  $CO<sub>2</sub>$  and the framework  $(2.3 \text{ Å})$ , indicating the weaker binding affinity of the framework with  $C_2H_2$ . The special binding configurations of  $CO_2$  and  $C_2H_2$  in  $Ce^{IV}$ -MIL-14-4F demonstrate the efficiency of the constructive strategy for  $CO_2$ -selective sorbents. A similar binding mode for  $C_2H_2$  on site II was observed in  $Zr^V$ -MIL-140-4F with distances of 2.7–3.1 Å. Furthermore, the host-guest interaction between  $C_2H_2$  and  $Zr^{IV}$ -MIL-140-4F was consolidated by the  $\pi \cdot \pi$  interaction between benzene ring on TFBDC and the triple bond on  $C_2H_2$  $(3.3 \text{ Å}, \text{Figure 3 f})$ . Similarly, CO<sub>2</sub> also located on site II with distances of 2.8–3.2 A, shorter than that of  $C_2H_2$ , and no interactions between benzene rings and  $CO<sub>2</sub>$  were observed (Figure S24). The binding energy of  $Zr^{IV}$ -MIL-140-4F for  $C_2H_2$  predicated by DFT calculations is 39.5 kJ mol<sup>-1</sup>, higher than that of  $CO<sub>2</sub>$  (33.1 kJ mol<sup>-1</sup>). This is consistent with the adsorption isotherms that Zr-MIL-140-4F exhibits the preferential adsorption ability for  $C_2H_2$  over  $CO_2$ .

To evaluate the feasibility of  $Ce^{IV}$ -MIL-140-4F for selective inverse  $CO_2/C_2H_2$  separation, transient breakthrough simulations were performed in fixed-bed adsorption processes.<sup>[19]</sup> The results show that highly efficient separations can be



 $\bm{\mathsf{Figure 3.}}$  a) Experimental in situ and refined PXRD patterns of CO $_2$ -loaded Ce $^{\text{IV}}$ -MIL-140-4F. b,c) Refined structure of CO $_2$ -loaded Ce $^{\text{IV}}$ -MIL-140-4F with CO<sub>2</sub> strongly bound by four F atoms. d) In situ FTIR spectra of the activated and CO<sub>2</sub>-loaded Ce<sup>IV</sup>- and Zr<sup>IV</sup>-MIL-140-4F. e) The binding site of  $\mathsf{C_2H_2}$  in Ce $^{\mathsf{IV}}$ -MIL-140-4F. f) The DFT-calculated binding configuration of  $\mathsf{C_2H_2}$  in Zr $^{\mathsf{IV}}$ -MIL-140-4F.

accomplished by Ce<sup>IV</sup>-MIL-140-4F for  $CO_2/C_2H_2$  (1/1 and 1/2) mixtures at  $273$  and  $298$  K, with high-purity  $C_2H_2$  harvested via a one-step breakthrough experiment (Figure 4 a; Figure S25a). The calculated productivity of high-purity  $C_2H_2$  $(>99\%)$  can reach 132.2 and 66.6 m<sup>3</sup>L<sup>-1</sup> at 273 K and 298 K, respectively, much higher than that on  $PCP-NH_2$ -ipa  $(28.5 \text{ m}^3 \text{L}^{-1})$ .<sup>[17]</sup> We further carried out the experimental breakthrough studies with  $CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub>$  (1/1 and 1/2) mixtures flowed over a Ce<sup>IV</sup>-MIL-140-4F-packed column at 273 and

298 K (Figure 4b; Figure S25b). A clear separation of  $CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub>$  mixtures was realized, which is consistent with the simulated breakthrough results.  $C_2H_2$  eluted through the column first to yield an outflow of pure  $C_2H_2$  (> 99.99%) with an undetectable amount of  $CO<sub>2</sub>$  in a single breakthrough operation. Notably, this is difficult for  $C_2H_2$ -selective adsorbents in the desorption process due to the co-adsorption of  $C_2H_2$  and  $CO_2$ . Furthermore,  $CO_2$  can be efficiently retained in the column for long periods with the dynamic capture



**Figure 4.** a) Simulated and b) experimental breakthrough curves for CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub> (1/1) separation in a fixed bed packed with Ce<sup>IV</sup>-MIL-140-4F at 273 and 298 K. c) Simulated and experimental breakthrough curves of C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> (1/1) mixture on Zr<sup>IV</sup>-MIL-140-4F at 298 K. All the simulated and experimental breakthrough curves were investigated at 1 bar with a flow rate of 2 mLmin<sup>-1</sup>.

amounts of 136.9 and  $99.7 \text{ cm}^3 \text{ cm}^{-3}$  at 273 and 298 K, respectively. Such a high working capacity is coincident with the  $CO_2$  adsorption isotherms. Moreover, the  $CO_2/C_2H_2$ separation performance was unimpeded by humidity (Figure S26), which may be due to the hydrophobic pore channels. The remarkable roll-up phenomenon on  $C_2H_2$  curves indicates strong competitive sorption of  $CO_2$  over  $C_2H_2$  on  $Ce^{IV}$ -MIL-140-4F. The separation factors for  $CO_2/C_2H_2$  (1/1) mixtures calculated from breakthrough experiments are 4.9 and 5.6 at 298 and 273 K, respectively. In contrast,  $Zr^{\text{IV}}$ -MIL-140-4F exhibits good separation performance for  $C_2H_2/CO_2$ mixtures (Figure 4c). Last but not least, the cycle and regeneration capabilities of Ce<sup>IV</sup>-MIL-140-4F were investigated (Figures S27 and S28). The results show that the column can be simply regenerated by purging He at room temperature. The inverse  $CO_2/C_2H_2$  separation capability of  $Ce^{IV}$ -MIL-140-4F was well retained with no noticeable decrease observed, confirming its good stability for inverse  $CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub>$ separation. The above results demonstrate that  $Ce<sup>IV</sup>-MIL-$ 140-4F can be a promising adsorbent for inverse  $CO_2/C_2H_2$ separation with desirable high-purity  $C<sub>2</sub>H<sub>2</sub>$  obtained via a single separation operation.

### Conclusion

In summary, we judiciously realized the efficient inverse  $CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub>$  adsorption and separation with an ultramicroporous Ce<sup>IV</sup>-based MOF, Ce<sup>IV</sup>-MIL-140-4F. Owing to the unoccupied 4f orbitals of  $Ce^{IV}$  with a strong electron-withdrawing effect from the fluorinated linkers, Ce<sup>IV</sup>-MIL-140-4F exhibits optimal pore chemistry of negative electrostatic potential around four F atoms coming from two parallel linkers. This optimal pore environment can preferentially trap CO<sub>2</sub> through the strong F···C=O interactions. On the contrary,  $Zr^{\text{IV}}$ -MIL-140-4F only shows a normal  $C_2H_2/CO_2$  separation selectivity. The inverse  $CO_2$ -selective sorption behavior of  $Ce^{IV}$ -MIL-140-4F was revealed by in situ PXRD and FTIR experiments, as well as molecular calculations. Such unique pore chemistry endows  $Ce^{IV}$ -MIL-140-4F with benchmark inverse  $CO_2/C_2H_2$  separation performance. High-purity  $C_2H_2$ ( $>$  99.99%) can be directly obtained from  $CO_2/C_2H_2$  mixtures through a single adsorption procedure, which was confirmed by the detailed simulated and experimental breakthrough studies. The elaborate design strategy for pore chemistry based on the intrinsic nature or differences between molecules is an effective way to control the discrimination ability of porous materials. This work opens a new avenue for the design of advanced porous materials in gas separation.

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### Conflict of Interest

The authors declare no conflict of interest.

**Keywords:**  $CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub>$  separation  $\cdot$ inverse adsorption and separation · pore chemistry · quadrupole moments · ultramicroporous MOFs

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# Supporting Information

# Optimal Pore Chemistry in an Ultramicroporous Metal–Organic Framework for Benchmark Inverse  $CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub>$  Separation

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# **SUPPORTING INFORMATION**

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### <span id="page-9-0"></span>**Experimental Procedures**

### **Synthesis of Ce(IV)- and Zr(IV)-MIL-140-4F**

Ce(IV)-MIL-140-4F was synthesized according to the reported method.<sup>[1]</sup> A mixture of cerium ammonium nitrate ((NH<sub>4</sub>)<sub>2</sub>Ce(NO<sub>3</sub>)<sub>6</sub>, CAN, 0.548 g, 1 mmol) and tetrafluoroterephthalic acid (H<sub>2</sub>TFBDC, 0.238 g, 1 mmol) in deionized (DI) water (50 mL) was heated to 110 °C under stirring and refluxed for 24 h. The obtained yellow solid was filtered and washed with water and acetone. The solid was then dried under vacuum at 80 °C for 24 h, resulting in Ce(IV)-MIL-140-4F. Differently, Zr(IV)-MIL-140-4F was achieved by refluxing the mixtures of zirconium tetrachloride (ZrCl<sub>4</sub>, 0.233 g, 1 mmol) and H<sub>2</sub>TFBDC (0.238 g, 1 mmol) in acetonitrile (50 mL) at 120 °C under stirring for 48 h. The resulted slurry was centrifuged and washed with acetone three times, then dried under vacuum at 120 °C for 24 h, leading to Zr(IV)-MIL-140-4F.

### **Synthesis of Ce-UiO-66-4F**

Briefly, CAN (0.548 g, 1 mmol), H<sub>2</sub>TFBDC (0.238 g, 1 mmol), and acetic acid (6 mL) were dissolved in DI water (45 mL) in a roundbottom flask. The solution was heated to 110 °C under stirring and refluxed for 24 h. The obtained yellow solid was collected and washed three times with DI water and once with acetone. The solid was then dried at 80 °C for 24 h, resulting in Ce-UiO-66-4F.

### **Synthesis of Zr(IV)-MIL-140**

A mixture of 1,4-benzenedicarboxylic acid (H<sub>2</sub>BDC, 0.332 g, 2 mmol), ZrCl<sub>4</sub> (0.233 g, 1 mmol), and DMF (8 mL) was gently stirred and introduced into a 25 mL Teflon-lined steel autoclave. The autoclave was sealed and placed in an oven at 220 °C and kept for 16 h. The white solid was then filtered and dried at 100 °C for 12 h, leading to Zr(IV)-MIL-140.

### **Synthesis of Ce(IV)-MIL-140**

Briefly, CAN (0.274 g, 0.5 mmol) and H<sub>2</sub>BDC (0.249 g, 0.75 mmol) were dissolved in acetonitrile (10 mL), then introduced into a microwave glass reactor (25 mL). The reactor was sealed and heated for 4 h at 140 °C. After cooling down to room temperature, the yellow product was filtered off, washed with acetone three times. The solid was then dried under vacuum at 100 °C for 12 h, resulting in Ce(IV)-MIL-140.

### **TGA measurements**

Thermogravimetric analyses (TGA) were performed on TA Instruments STD-600 at a heating rate of 10 K min-1 up to 800 °C with an  $N_2$  flow rate of 50 mL min<sup>-1</sup>. The sample holders were alumina crucibles, and the amount of sample used in each measurement was 10  (± 2) mg. The data collected were analyzed using Universal Analysis software (version 4.4A) from TA Instruments.

### **Gas sorption experiments**

Adsorption and desorption experiments of  $CO<sub>2</sub>$  and  $C<sub>2</sub>H<sub>2</sub>$  were performed at different temperatures on a Micromeritics ASAP 2020 instrument equipped with commercial software for data calculation and analysis. The test temperatures were controlled by soaking the sample cell into a circulating water bath (298 K) or ice water bath (273 K). Before measurement, the sample (80–100 mg) was degassed at 373 K for 12 h. The gas isotherms were obtained under a pressure range of 0–100 kPa. CO<sub>2</sub> and N<sub>2</sub> isotherms at 196 K and 77 K, respectively, were also collected on a Micromeritics ASAP2020 instrument. The measurement temperatures were maintained at 195 and 77 K using dry ice/acetone and liquid nitrogen, respectively.

### **Powder X-ray diffraction analyses**

Powder X-ray diffraction (PXRD) patterns were collected using a Rigaku Miniflex 600 diffractometer (Cu Kα *λ* = 1.540598 Å) with an operating power of 40 kV, 15 mA, and a scan rate of 2.0 ° min<sup>-1</sup>. The data were collected in a two-theta range of 5–40°. In situ PXRD patterns were collected with a chamber holding the sample, which was firstly evacuated and then filled with  $CO<sub>2</sub>$  gas. Pawley refinement was performed on the obtained PXRD data using the Reflex Module in *Materials Studio* software. Due to the abundant atoms in the crystal unit cell, the ligand molecule and the gas molecule were both treated as rigid bodies during the Pawley refinements, with the molecule orientation and center of mass freely refined. Final refinement on the positions/orientations of the rigid bodies, thermal factors, occupancies, lattice parameters, background, and profiles converged with satisfactory *R*-factors.

### **In situ Fourier transform infrared spectroscopy**

The *in situ* Fourier transform infrared (FTIR) spectra were recorded using an FTIR spectrometer (Bruker VERTEX 70-FTIR). Before each experiment, the sample (∼100 mg) was pretreated under high vacuum conditions (< 3 μmHg) at 393 K for 6 h, and then cooled to room temperature. The sample was then exposed to  $CO<sub>2</sub>$  with a pressure of 1.0 bar for 24 h to ensure that the adsorption has reached equilibrium. Then the sample was used for FTIR measurements. All the spectra were recorded over accumulative 32 scans with a resolution of 4 cm<sup>-1</sup> in the range of 4000–400 cm<sup>-1</sup>.

### **Breakthrough experiments**

The breakthrough experiments were performed using a home-built dynamic gas breakthrough setup. The experiment was conducted using a stainless-steel column (4.6 mm inner diameter x 50 mm length). Before the breakthrough experiment, the column packed with Ce(IV)- or Zr(IV)-MIL-140-4F (0.55 or 0.5 g, respectively) was firstly activated with a He flow (5 mL min<sup>-1</sup>) at 423 K for 12 h. After activation, the gas mixture (C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub>, volume ratio of 1/1 or 2/1) was introduced, and outlet gas from the column was monitored by a

mass spectrometer (Hiden QGA quantitative gas analysis system). After the breakthrough experiment, the sample was regenerated with a He flow (5 mL min<sup>-1</sup>) at 373 K. Before each cyclic experiment, the sample was activated by heating at 100 °C for 6 h.

#### **Breakthrough simulations**

Transient breakthrough simulations were performed using the simulation methodology described previously.[2] The breakthrough experiments were conducted in a tube of diameter  $d = 4.6$  mm and length  $L = 0.05$  m. The mass of the crystallites in the packed tube is  $m_{ads}.$  For a crystal framework density of  $\rho$  kg m<sup>-3</sup>, we calculated  $(1 - \varepsilon) =$  $\frac{m_{ads}}{m_{\pi}^{2}L}$  and  $\varepsilon = 1 -$ 4 4 Ce(IV)-MIL-140-4F and Zr(IV)-MIL-140-4F are 2170 kg m-3 and 2050 kg m-3 , respectively. The total flow rate of the gas mixture at the  $\frac{m_{ads}}{r_{\pi d^2 L}}$ . The crystal framework densities of entrance  $Q_0$  = 2 mL min<sup>-1</sup> = 3.333 x 10<sup>-8</sup> m<sup>3</sup> s<sup>-1</sup>. The superficial gas velocity at the inlet to the adsorber  $u=\frac{Q_0}{\pi d^2}$ . The interstitial velocity 4

 $v=\frac{Q_0}{\varepsilon rad^2}$ . The breakthrough simulations were performed for a total gas pressure of 100 kPa, with a constant temperature of 273 or 298 4

K. During the initial transience, the effluent gas contains pure  $C_2H_2$ , and this continues until  $CO_2$  starts breaking through because its uptake capacity in the MOF has been reached. During a certain interval,  $\tau_{break}$ , pure  $C_2H_2$  can be recovered in the gas phase. The desired purity level for C<sub>2</sub>H<sub>2</sub> was set at say 99%+, then the number of moles of C<sub>2</sub>H<sub>2</sub> purged during the time intervals 0 to  $\tau_{break}$ , can be determined from a material balance. Dividing the purged number of moles of  $C_2H_2$  by the mass of adsorbent in the bed,  $m_{ads}$ , yields the productivity of C<sub>2</sub>H<sub>2</sub> (mol kg<sup>-1</sup>). The gravimetric CO<sub>2</sub> uptake capacity, expressed in mol kg<sup>-1</sup>, can be determined from a material balance.

#### **DFT calculations**

First-principles density functional theory (DFT) calculations were performed in Castep software (*BIOVIA Materials Studio*).[3] A semiempirical addition of dispersive forces to conventional DFT was included in the calculation to account for van der Waals inte ractions. Vanderbilt-type ultra-soft pseudopotentials and generalized gradient approximation with Perdew–Burke–Ernzerhof exchange correlation were used. A cutoff energy of 590 eV and a 1 × 1 × 2 *k*-point mesh (generated using the Monkhorst-Pack scheme) were found to be enough for the total energy to converge within 0.01 meV atom<sup>-1</sup>. The structures of the synthesized materials were firstly optimized, then various guest gas molecules were introduced to various locations of the channel pore, followed by a full structural relaxation. To obtain the gas binding energy, an isolated gas molecule placed in a supercell (with the same cell dimensions as the material crystal) was also relaxed as a reference. The static binding energy (at  $T = 0$  K) was then calculated using:  $E_B = E_{(MOF)} + E_{(gas)}$ *- E(MOF + gas)*.

### **IAST selectivity calculations**

The isotherm data for  $CO<sub>2</sub>$  and  $C<sub>2</sub>H<sub>2</sub>$  were fitted with dual-site Langmuir-Freundlich isotherm model:<sup>[4]</sup>

$$
q = q_{A,sat} \frac{b_A p^{\nu_A}}{1 + b_A p^{\nu_A}} + q_{B,sat} \frac{b_B p^{\nu_B}}{1 + b_B p^{\nu_B}}
$$
(1)

With T-dependent parameters *b*:

$$
b = b_0 \exp\left(\frac{E}{RT}\right) \tag{2}
$$

The adsorption selectivity for  $CO_2/C_2H_2$  separation is defined by:

$$
S_{ads} = \frac{q_1/q_2}{p_1/p_2} \tag{3}
$$

Where *q<sup>1</sup>* and *q<sup>2</sup>* are the molar loadings in the adsorbed phase in equilibrium with the bulk gas phase with partial pressures *p<sup>1</sup>* and *p2*.

#### **Isosteric heat of adsorption calculations**

A virial-type expression comprising the temperature-independent parameter *a<sup>i</sup>* and *b<sup>j</sup>* was employed to calculate the heat of adsorption for different gases (at different temperatures). In each case, the data were fitted using the equation:[5]

$$
\ln P = \ln N + 1/T \sum_{i=0}^{m} a_i N^i + \sum_{j=0}^{n} b_j N^j \tag{4}
$$

Here, P is the pressure expressed in Pa, N is the amount adsorbed in mmol g<sup>-1</sup>, T is the temperature in K, a*i* and b<sub>*i*</sub> are virial coefficients, and *m*, *n* represent the number of coefficients required to adequately describe the isotherms.

The values of the virial coefficients  $a_0$  through  $a_m$  were then used to calculate the isosteric heat of adsorption using the following expression:

$$
Q_{st} = -R \sum_{i=0}^{m} a_i N^j \tag{5}
$$

*Qst* is the coverage-dependent isosteric heat of adsorption and *R* is the universal gas constant.

### <span id="page-11-0"></span>**Supplementary Figures**



Figure S3. TGA curves of various materials collected with a heating rate of 10 K min<sup>-1</sup> and an N<sub>2</sub> flow rate of 50 mL min<sup>-1</sup>.



**Figure S4.** Experimental PXRD patterns of Ce(IV)-MIL-140-4F before and after disposition under various conditions.



Figure S5. CO<sub>2</sub> sorption isotherms on Ce(IV)-MIL-140-4F after different treatments at 298 K.













**Figure S9.** PXRD patterns of activated and CO2-loaded Ce-UiO-66-4F.



Figure S10. CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> adsorption isotherms of Zr(IV)-MIL-140-4F collected at 273 and 298 K.



**Figure S11.** CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> adsorption isotherms of Ce-UiO-66 collected at 273 and 298 K.



Figure S12. CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> adsorption isotherms of Ce-UiO-66-4F collected at 273 and 298 K.



Figure S13. CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> adsorption isotherms of Zr-UiO-66-4F collected at 273, 298, and 313 K.



Figure S14. CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> adsorption isotherms of TIFSIX-3-Ni and GeFSIX-3-Ni at 298 K.



**Figure S15.** IAST adsorption selectivity for equimolar C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> mixture of Ce(IV)/Zr(IV)-MIL-140-4F, and GeFSIX-3-Ni.



Figure S16. IAST adsorption selectivity for CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub> (1/2) mixture of Ce(IV)-MIL-140-4F.



Figure S18. The virial fitting of C<sub>2</sub>H<sub>2</sub> and CO<sub>2</sub> sorption isotherms for Ce(IV)-MIL-140-4F (a and b) and Ce-UiO-66-4F (c and d).



Figure S19. The virial fitting of C<sub>2</sub>H<sub>2</sub> and CO<sub>2</sub> sorption isotherms for Zr(IV)-MIL-140-4F (a and b) and Zr-UiO-66-4F (c and d).



**Figure S20.** In situ FTIR spectra of activated and CO<sub>2</sub>-loaded Ce(IV)-MIL-140.



**Figure S21.** In situ FTIR spectra of activated and CO<sub>2</sub>-loaded Ce-UiO-66-4F.



**Figure S22.** In situ FTIR spectra of activated and CO<sub>2</sub>-loaded Zr(IV)-MIL-140-4F.







Figure S24. DFT-calculated configuration of CO<sub>2</sub> in the pore channel of Zr(IV)-MIL-140-4F.



**Figure S25.** Simulated (a) and experimental (b) breakthrough curves for CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub> (1/2) mixture on Ce(IV)-MIL-140-4F at 273 and 298 K. Note: All the simulated and experimental breakthrough curves were investigated at 1 bar with a flow rate of 2 mL min<sup>-1</sup>.



Figure S26. Breakthrough curves for CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub> (1/1) mixture on Ce(IV)-MIL-140-4F with 72% humidity at 298 K with a flow rate of 2 mL min<sup>-1</sup>.



**Figure S27.** Desorption curves of C<sub>2</sub>H<sub>2</sub> and CO<sub>2</sub> from Ce(IV)-MIL-140-4F-packed column collected by purging He with a flow rate of 10 mL min-1 at 298 K.



**Figure S28.** Multiple-cycle breakthrough tests of Ce(IV)-MIL-140-4F for CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub> (1/1) separation at 273 K.



**Figure S29.** Schematic illustration of the breakthrough setup used in this study.

## <span id="page-25-0"></span>**Supplementary Tables**





Table S2. Dual-site Langmuir-Freundlich parameter fits for CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> of different materials.

		Site A			Site B		
		<b>GA</b> ,sat	bд	VA	$q_{B,sat}$	$b_B$	VB
		mol $kg^{-1}$	$Pa^{-vA}$		mol kg <sup>-1</sup>	$Pa^{-vB}$	
Ce(IV)-MIL-140-4F	CO <sub>2</sub>	1.7	5.737E-05		1.7	1.585E-18	5.2
(273 K)	$C_2H_2$	1.2	6.892E-05		0.7	6.283E-07	
Ce(IV)-MIL-140-4F	CO <sub>2</sub>	1.6	2.025E-05		1.2	2.104E-19	4.6
(298 K)	$C_2H_2$	0.35	3.904E-06		1.4	1.138E-05	
GeFSIX-3-Ni	CO <sub>2</sub>	1.16	3		2.50	1.098	
(298 K)	$C_2H_2$	1.54	28.99		1.54	28.99	
Zr(IV)-MIL-140-4F	CO <sub>2</sub>	1.2	7.493E-06		1.2	7.493E-06	
(298 K)	$C_2H_2$	5	3.744E-06		0.8	7.301E-05	

**Table S3.** List of atomic positions for CO<sub>2</sub>-loaded Ce(IV)-MIL-140-4F.





# **SUPPORTING INFORMATION**



### **Table S4.** List of atomic positions for Zr(IV)-MIL-140-4F.







### <span id="page-30-0"></span>**Supplementary Movie Titles**

Movie S1. Development of CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> concentration along the length of the fixed bed of Ce(IV)-MIL-140-4F at 273 K. Movie S2. Development of CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> concentration along the length of the fixed bed of Ce(IV)-MIL-140-4F at 298 K. **Movie S3.** Development of gas phase concentration along the length of the fixed bed of Zr(IV)-MIL-140-4F at 298 K.

### <span id="page-31-0"></span>**References**

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